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Research article

Analysis and simulation of sub-synchronous resonance in steam turbine on a series-compensated network

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Abstract

In series compensation networks (where capacitors are added to transmission lines to improve power transfer), transient events (such as faults or disturbances) can amplify the torque on the turbine generator shafts. Series capacitors are used to increase the power transfer capability by compensating for some of the reactance in the transmission lines. The use of series capacitors may cause the phenomenon of sub-synchronous resonance (SRR). This phenomenon may cause torsional oscillations in the turbine-generator shaft system and electrical oscillations with sub-synchronous frequency. In this paper, the objective is to study and analyze the phenomenon of sub-synchronous resonance in a steam turbine in a series compensated power system. The system has a synchronous generator connected to an infinite bus via two transmission lines, one with series compensation. A three-phase fault followed by fault recovery excites the torsional modes of the system, leading to a potential torque amplification on the generator shaft. The mechanical system is modeled as a three-mass system consisting of a generator, a low-pressure turbine, and a high-pressure turbine. The system starts in steady state. A three-phase fault is considered for 0.017 seconds (starting at 0.1 seconds). This excites torsional modes and leads to oscillations in the shaft torques. Increasing the compensation percentage reduces the series capacitor voltage and phase current, but increases the magnitude of the oscillations in the masses and mass velocities. The simulation results are shown using the MATLAB Simulink implementation of the studied system model.

Keywords: Compensation network, Multi-mass shaft, Steam turbine, Sub-synchronous resonance.

1- Introduction

In recent years, the development and application of renewable energy generation technologies have been expanding [1-3]. The rapid increase in the penetration of renewable energy due to its high availability and security indicates that renewable energy is becoming a major

energy source. The expansion of renewable energy can effectively reduce the concern of energy demand. The expansion of power electronics-based energy generation will cause changes in the dynamic characteristics of the power system, which will lead to increased susceptibility to subsynchronous oscillations (SSO) [4-11].

Power system outages can actually be caused by insufficient oscillation damping, which can lead to instability subsequent failures. Sub-synchronous oscillation in power systems can be amplified and sustained due to physical interactions, which involve the exchange of energy between two power facilities [12,13]. Such phenomena are called subsynchronous interactions (SSI) [14,15], which can be classified into synchronous torsional interactions (SSTI) sub-synchronous [16,17],control interactions (SSCI) [18,19], and subsynchronous resonance (SSR) [20,21]. Sub-synchronous oscillation is a harmful phenomenon, and it exhibits oscillations with a frequency of 5 to 55 Hz with a fundamental frequency of 60 Hz, and is different from low frequency oscillation (LFO) that occurs at around 0.5 Hz to 3 Hz. Sub-synchronous oscillation involves simultaneous oscillations between two or more power system elements. Subsynchronous oscillations can cause instability in the operation of entire power therefore, systems, and there possibility of damaging the electrical equipment of the systems [22,23]. Methods for analyzing sub-synchronous oscillations can be divided into two groups: frequency domain analysis and time simulation methods [24,25]. Sub-synchronous oscillations include torsional interference with power system controls, torsional fatigue tolerance due to network switching, and sub-synchronous resonance. Subsynchronous resonance is a condition of an electric power system, in which the electrical network exchanges significant energy with a generator-turbine at one or more natural frequencies of the system below the synchronous frequency of the

power system [26,27]. There are three types of sub-synchronous resonances: induction generator effect (SSR-IGE), torsional interaction (SSR-TI), and torque amplification (SSR-TA) [28,29]. classification of sub-synchronous resonance is shown in Fig. 1 [30]. SSRinvolves purely electrical excitation without significant mechanical interference. This occurs when synchronous currents in the generator armature create a rotating magnetic field that induces voltages in the rotor at subsynchronous frequency. In steam turbines, IGE is more likely in systems with high series compensation, where the generator behaves like an induction generator at subsynchronous frequencies, potentially sustaining unstable currents.

SSR-TI is the most common and severe form of SSR in steam turbines, involving the coupled interaction between mechanical torsional modes of the turbine shaft and the electrical network. Steam turbines are particularly vulnerable due to their large shaft masses and low damping in certain modes, often caused by network disturbances such as faults. SSR-TA is caused by large transient disturbances in the network, such as short circuits or switching events. This type causes sudden, high-magnitude torque pulses on the shaft that can be amplified if the complement of the electrical resonance frequency is aligned with the torsional mode. In steam turbines, SSR-TA is a concern in highly compensated lines, where peak torques can double or more compared uncompensated systems [31-35].

Sub-synchronous resonance can be caused by series compensated lines, which will lead to damage to the turbo-generator shaft [36,37].

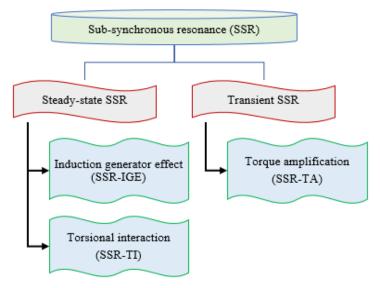


Fig. 1 Sub-synchronous resonance classification

Literature review

Any power system condition where energy exchange at a given sub-synchronous frequency is possible may cause SSR oscillations. There are many ways in which the system and the generator can interact at sub-synchronous frequencies. increasing penetration of renewable energy sources has led to the widespread use of series compensators. Series compensated capacitors in AC transmission lines not only increase the overall load carrying capacity of the system, but also improve transient stability and power control, and reduce losses. However, capacitors can cause sub-synchronous resonance due to their interaction with turbine generators, which can lead to shaft failure. The phenomenon of sub-synchronous resonance (SSR) in series compensated transmission networks has been investigated in various studies [38-41]. A number of studies are mentioned in this section.

Sub-synchronous resonance in power systems where a steam turbine-generator is connected to a long transmission line with series compensation is investigated in [42], which evaluates the distributed static series

compensator (DSSC) [a device from the distributed flexible ac transmission system (D-FACTS) family] as a mitigation tool, enhanced with advanced controllers. Two controllers (PSO-based CDC and FLBDC) are designed for DSSC to effectively suppress SSR. The performance of each controller is evaluated under normal and fault conditions. Α custom performance index (PI) is considered to quantify the damping effectiveness based on the power system dynamics. Simulation results show that FLBDC outperforms PSO-based CDC by providing superior damping and stability, especially in severe transient scenarios.

A solution for suppressing subsynchronous resonance in wind farms under weak grid conditions, which is caused by impedance interactions between the wind farm and the grid, is discussed in [43], where a synchronous compensator with a battery energy storage system (STATCOM/BESS) connected to the grid in parallel is used to mitigate SSR. A virtual synchronous generator strategy is used to increase grid rigidity. This strategy

allows the STATCOM/BESS to operate with low rated active power and high rated reactive power, reducing the battery capacity requirement by more than 50%. This reduction reduces costs and improves system security. The control strategy ensures that the grid and STATCO-M/BESS impedances are primarily inductive, resulting in a lower parallel impedance compared to the grid alone, effectively increasing the grid rigidity from an impedance perspective.

Torque amplification can lead to excessive loss of fatigue life or sudden shaft failure. A scheme for instantaneous transient torque protection is presented in [44], which is designed to increase the safety of turbine generator shafts in power networks with series compensation. In this method, real-time shaft speed measurements are used to estimate the transient torque. The estimated torque is compared with predefined trip thresholds to decide whether to trip the generator and prevent damage.

The ability of power converters in doubly fed induction generator wind farms to reduce the effects of sub-synchronous resonance has been investigated in [45], where the design of the auxiliary SSR damping controller and the selection of control signals have been considered. Simulation results using MATLAB Simulink show simultaneous improvement of both sub-synchronous and supersynchronous resonance modes.

The graphical state space-based impedance modeling method in [46] is used to determine the accurate impedance model of the thermal power unit, which includes the shaft torsion characteristics. The responses of each torsion mode of the thermal power unit to the wind force fluctuation are analyzed in time domain simulation. The simulation results show

that the possibility of torsional oscillation is possible when the wind power oscillation frequency approaches the torsional mode frequency, but the risks will be different in different torsional modes, which can be investigated through the shaft torsion characteristics in the thermal power unit's impedance.

The phenomenon of sub-synchronous oscillations in a wind farm based on doubly fed induction generators investigated in [47]. The voltage waveform recorded during the sub-synchronous resonance event is analyzed, and then an equivalent model of the system including the wind farm, static synchronous compensator, and power grid determined. The simulation results provide a criterion for the occurrence of subsynchronous resonance in the time domain and spectrum analysis.

A method for enhancing SSR detection by combining the frequency analysis of the generator magnetic flux linkage (an electrical signal) with the shaft speed (a mechanical signal) is presented in [48]. In this method, the magnetic flux linkage provides a local and easily accessible indicator without the need for communication channel, but its use requires invasive sensors.

Sub-synchronous resonance compensated power systems has been investigated in [49], where the influence of various parameters on the torsional mode damping is shown. In this study, eigenvalue analysis, validated with PSCAD simulations, is used to evaluate the effects of series compensation levels, parameters, speed control generator systems, and excitation systems on the characteristics of SSRs. The simulation results show the dominant influence of series compensation levels on torsional

mode damping, such that the generator, speed control, and excitation system parameters play a role, especially in low-frequency oscillations.

Structure of the paper

Sub-synchronous resonance occurs when, between the electrical resonance frequency fer and the synchronous frequency fs, the complementary frequency (the difference between the two frequencies f_s and f_{er}) matches the rotor frequency. As the level of transmission line compensation increases, the resonance point will move towards the system frequency, exposing the power plant to potential problems of sub-synchronous resonance. synchronous resonance can cause sustained or increasing oscillations that potentially lead to turbine-generator shaft failure due to fatigue. In this paper, the aim of the study of sub-synchronous resonance in a steam turbine in a compensated network is to study.

The power system under study consists of a synchronous generator connected to an infinite bus through two transmission lines. To investigate the effect of series compensation, one of the two parallel lines is compensated with a capacitor. By implementing the power system under study in the MATLAB Simulink environment, the simulation results in the time domain for different synchronisms are shown. The simulation results show the speed deviations and torques transmitted between the shaft masses.

The highlights of this study include the following:

- The phenomenon of sub-synchronous resonance in a series compensated power system connected to an infinite bus via two lines, one with series compensation, has been analyzed.

- The effect of compensating series capacitor on sub-synchronous oscillations is shown.
- The effects of transmission line impedance changes on simulation results are investigated.

The structure of the paper is as follows. In the section 2, the model of the power system under study is shown. In the section 3, the analysis and discussion of the simulation results using MATLAB software are presented. Finally, in the section 4, conclusions and suggestions for further research are expressed.

2- Model of the studied power system

Sub-synchronous resonance is a phenomenon in which the electrical network of the power system interacts with the mechanical system (turbine-generator shaft) at frequencies lower than the synchronous frequency of the system. Adding series the transmission lines capacitors to increases their power transfer capability. However, it can also cause sub-synchronous resonance. The interaction between the electrical and mechanical systems during sub-synchronous resonance can cause the generator shaft to experience amplified torsional oscillations, potentially leading to damage [50,51].

The studied power system consists of a single synchronous generator connected to an infinite bus via two parallel transmission lines (Fig. 2). One of the transmission lines is compensated using a series capacitor. After applying and removing the three-phase fault, series compensation can induce sub-synchronous oscillations, which can lead to torque amplification in the multi-mass shaft. The turbine-generator shaft is considered as a system of three

interconnected masses, namely: a generator, a low-pressure turbine, and a high-pressure turbine.

In turbines with long lengths, there is a possibility that different parts will have different angles relative to each other. A steam turbine is made up of various parts, and the discussion of torsional oscillations is very important in it. Torsional oscillations are modeled by choosing the angles of different parts of the system as follows:

$$\frac{d^2}{dt^2}\theta = -[K]\theta\tag{1}$$

where K is stiffness coefficient matrix of the system and θ are the angle vectors of the masses forming the system. The eigenvectors of the K matrix show how the natural frequencies are distributed on the rotor. Also, the eigenvectors of the K matrix show how the natural frequencies are distributed on the rotor.

The natural frequency (torsional oscillation frequency) of the ith mode is determined by the eigenvalues of the mass stiffness coefficient matrix, and is given in Hz by the following equation:

$$f_{i} = \frac{\sqrt{2\pi f_{b} |\lambda_{i}|}}{2\pi} \tag{2}$$

where f_b is the nominal frequency and λ_i is the i^{th} eigenvalue of the stiffness coefficient matrix of the system. In the system under study, considering three masses, the stiffness coefficient matrix will have three eigenvalues.

The zero mode represents a free rotating body, and when the generator is connected to the system, the frequency of this mode increases, which is the rotor oscillation frequency. Ignoring the rotational friction coefficient and considering the angles of the three different masses of the high-pressure turbine (θ_{HP}), low-pressure turbine (θ_{LP}), and generator (θ_{G}), the equations of torsional oscillations are expressed as follows:

$$\ddot{\theta} = -\begin{bmatrix} \frac{K_{H-L}}{J_{HP}} & -\frac{K_{H-L}}{J_{HP}} & 0\\ -\frac{K_{H-L}}{J_{LP}} & \frac{K_{H-L} + K_{L-G}}{J_{LP}} & -\frac{K_{L-G}}{J_{G}} \\ 0 & -\frac{K_{L-G}}{J_{G}} & \frac{K_{L-G}}{J_{G}} \end{bmatrix} \theta$$

$$\theta = \begin{bmatrix} \theta_{HP} & \theta_{LP} & \theta_{GE} \end{bmatrix}^{T}$$

$$(3)$$

3- Analysis and discussion of simulation results

When the electrical resonance frequency of the system, under the influence of the series capacitor, matches or is close to the mechanical resonance frequency of the turbine-generator shaft, the system susceptible SSR. becomes to This frequency matching allows energy exchange between the electrical and mechanical systems at sub-synchronous frequencies. The system under study consists of a 600 MVA, 22 kV, 60 Hz, 3600 rpm generator connected to an infinite bus through two transmission lines, one of which is a 55% series compensated transmission line. The reactance of the series capacitor is 0.08 per unit.

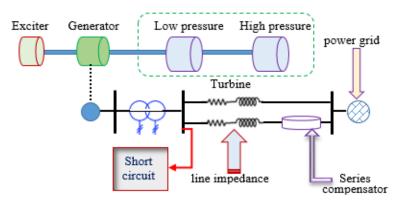


Fig. 2 Diagram of the studied power system

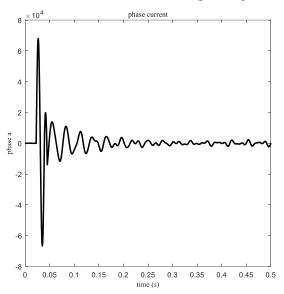
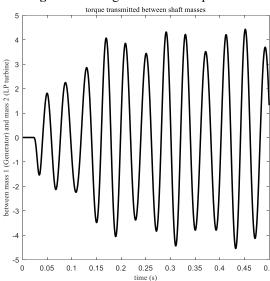
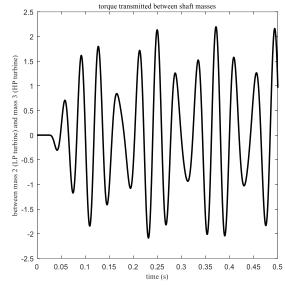


Fig. 3 The changes in current in phase a



(a) Generator and low pressure turbine masses



(b) Low pressure turbine and High pressure turbine masses

Fig. 4 Torque between different masses

Table 1: Base parameters

Parameters	Value	Unit
Base voltage (Vrms ph-ph)	500	KV
Frequency	60	Hz
Base power	100	MVA
Base impedance	2500	Ω
Base current	200	A
Base inductance	6.6315	Н
Base capacitor	9.42×10 ⁵	F

The sub-synchronous state created by the compensation capacitor after applying and removing the three-phase fault excites the oscillating torsional modes of the multimass shaft, and the torque amplification phenomenon is observed. The mechanical system is modeled with three masses, which include the generator (mass 1), the

low-pressure turbine (mass 2), and the high-pressure turbine (mass 3).

The nominal speed of the synchronous machine is 3600 rpm. The base values are given in Table 1. The changes in phase a current are shown in Fig. 3. The torque between the masses of the generator-medium pressure turbine and the medium pressure turbine-low pressure turbine is shown in Fig. 4. As can be seen, the peak torque between masses 1 and 2 is more than 4 per unit and the peak torque between masses 2 and 3 is more than 2 per unit. The changes in the fault current in phase a are shown in Fig. 5.

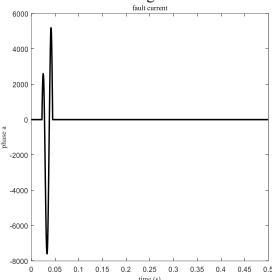
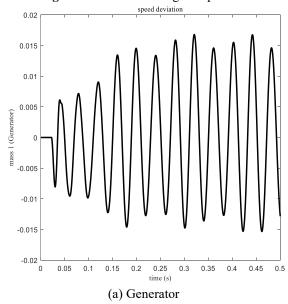
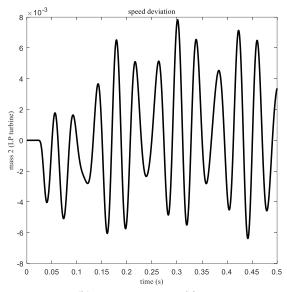
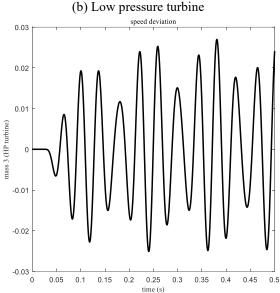


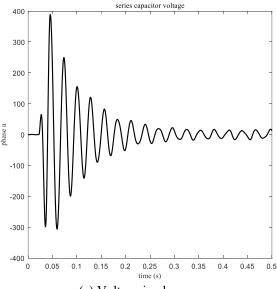
Fig. 5 Fault current changes in phase a



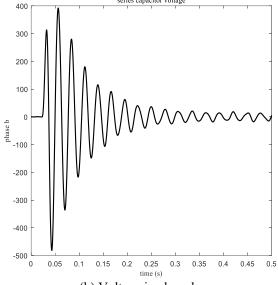


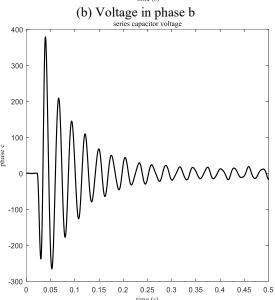


(c) High pressure turbine **Fig. 6** Speed changes in different masses

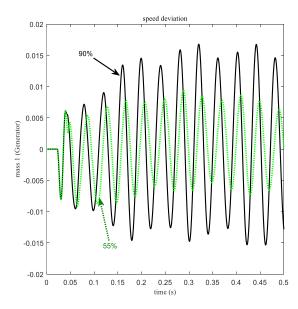


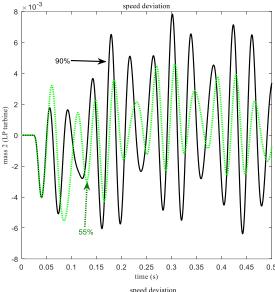
(a) Voltage in phase a





(c) Voltage in phase c
Fig. 7 Series capacitor compensation voltage





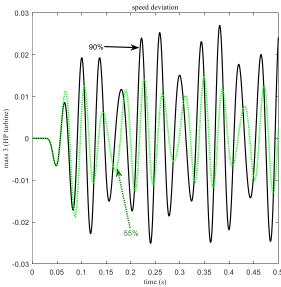


Fig. 8 The effect of compensation changes on the speed of different masses

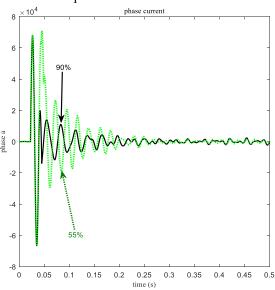


Fig. 9 Effect of changing the compensation percentage on phase current

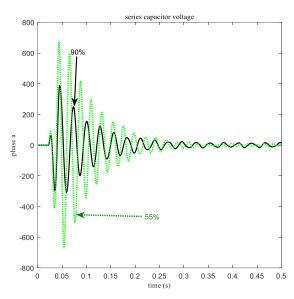


Fig. 10 Effect of changing the compensation percentage on series capacitor voltage

The changes in the speed of different masses are shown in Fig. 6. The series capacitor compensation voltage in different phases is shown in Fig. 7.

Fig. 5 shows the fault current passing through the fault impedance. It is natural that during the fault there is only current and after the fault is cleared the current will be cut off. But in Fig. 3 the phase current is shown. Phase a is in the circuit before and after the fault. After the fault is cleared the current in phase a progresses towards damping and will reach a permanent state.

The effect of varying the compensation on the velocities of the different masses is shown in Fig. 8. As can be seen, in general, increasing the compensation percentage will increase the size of the velocity fluctuations in the three masses, and will not have much effect on the period of the fluctuations.

Figures 9 and 10 show the current in phase a and the series capacitor voltage in phase a, respectively. As can be seen, increasing the compensation percentage has reduced the magnitude of the phase current and the magnitude of the series capacitor voltage.

4- Conclusion

One of the methods to increase the efficiency of existing power systems is to use a series capacitor as a series compensator in the transmission system. Sub-synchronous resonance in seriescompensated transmission systems is a phenomenon in which electrical and mechanical oscillations at frequencies below the synchronous frequency can lead to instability and possible damage to turbine generators. This phenomenon occurs when the electrical system (including series compensation) and the mechanical system (turbine-generator) exchange energy at the resonant frequency.

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