

Theoretical analysis of a thermal plasma-loaded relativistic traveling wave tube having corrugated slow wave structure with solid electron beam

Zahra Javadi · Shahrooz Saviz

Received: 22 July 2014 / Accepted: 17 December 2014 / Published online: 10 January 2015
© The Author(s) 2015. This article is published with open access at Springerlink.com

Abstract A relativistic traveling wave tube with thermal plasma-filled corrugated waveguide is driven by a finite solid electron beam with the entire system immersed in a strong longitudinal magnetic field that magnetized plasma and electron beam. The dispersion relation for the relativistic traveling wave tube is obtained by linear fluid theory. The numerical results show that the growth rate decreases by increasing plasma temperature, waveguide radius, plasma density and electron beam energy. As show in this paper the effect of electron beam density and corrugation period is to increase growth rate.

Keywords RTWT · Solid electron beam · Thermal plasma · Dispersion relation · Growth rate

Introduction

Relativistic traveling wave tube (RTWT) is an important high-power microwave (HPM) apparatus which has been developed in the past 20 years [1–3]. Most of the TWT mathematical analysis has been done by John Robinson Pierce and his colleagues at Bell Labs [4–6] and then have been developed by Chu, Jackson and Freund [7–9]. In TWT, sinusoidal corrugated slow wave structure (SWS) is used to reduce the phase velocity of the electromagnetic wave to synchronize it with the electron beam velocity, so

that a strong interaction between the two can take place [10, 11]. TWT is extensively applied in satellite and airborne communications, radar, particle accelerators, cyclotron resonance and electronic warfare system. The plasma injection to TWT has been studied recently which can increase the growth rate and improve the quality of transmission of electron beam. We investigate the effect of thermal plasma and electron beam on the growth rate [12–17].

In this paper, RTWT with magnetized thermal plasma-filled corrugated waveguide with solid electron beam is studied. The dispersion relation of corrugated waveguide is derived from a solution of the field equations. By numerical computation, the dispersion characteristics of RTWT are analyzed in detail with different cases of various geometric parameters of slow wave structure.

In “[Physical model](#)”, the physical model of RTWT filled with thermal plasma is established in an infinite longitudinal magnetic field. In “[Dispersion equation](#)”, the dispersion relation of RTWT is derived. In “[Numerical result and discussion](#)”, the dispersion characteristics of the RTWT are analyzed by numerical computation.

Physical model

The analysis presented in this paper is based on the SWS shown in Fig. 1. The SWS is a sinusoidal cylindrical waveguide that consists of an axially symmetric.

$$R(z) = R_0 + h \cos(\kappa_0 z), \quad (1)$$

$$K_n = k_z + n\kappa_0, \quad (2)$$

$$\kappa_0 = \frac{2\pi}{z_0}, \quad (3)$$

Z. Javadi
Central Tehran Branch, Islamic Azad University, Tehran, Iran

S. Saviz (✉)
Plasma Physics Research Center, Science and Research Branch,
Islamic Azad University, Tehran, Iran
e-mail: azarabadegan@gmail.com

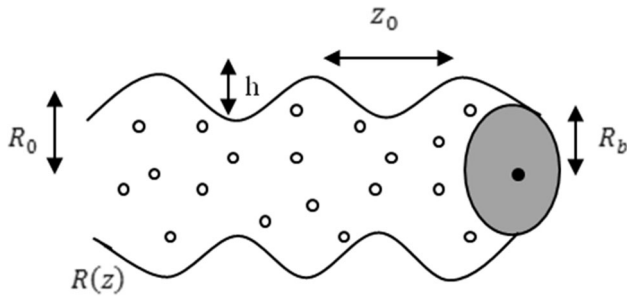


Fig. 1 Slow wave structure model of a plasma-filled relativistic traveling wave tube

Cylindrical waveguide, whose wall radius $R(z)$, varies sinusoidal according to the relation (1), h is the corrugation amplitude, $\kappa_0 = 2\pi/z_0$ is the corrugation wave number, and z_0 is the length of the corrugation period, R_0 is the waveguide radius and k_z is the axial number wave.

A finite solid relativistic electron beam with density n_b and radius R_b goes through the cylindrical waveguide, which is loaded completely with thermal, uniform and collisionless plasma of density n_p . The entire system is immersed in a strong, longitudinal magnetic field, which magnetizes both the beam and the plasma. Because of being anisotropic of dielectric constant it will be a tensor. In the beam-plasma case in a linearized scheme, the dielectric tensor in cylindrical coordinates may be given by:

$$[\varepsilon] = \varepsilon_0 \begin{bmatrix} \varepsilon_1 & \varepsilon_2 & 0 \\ -\varepsilon_2 & \varepsilon_1 & 0 \\ 0 & 0 & \varepsilon_3 \end{bmatrix}, \tag{4}$$

We assume that B_0 is very strong that $\varepsilon_1 = 1$ and $|\varepsilon_2|$ is negligibly small.

$$[\varepsilon] = \varepsilon_0 \times \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 - \frac{\omega_b^2}{\gamma^3(\omega - K_n v)^2 - 3K_n^2 v_{thb}^2} - \frac{\omega_p^2}{\omega^2 - 3K_n^2 v_{thp}^2} \end{bmatrix}, \tag{5}$$

$$\varepsilon_3 = 1 - \frac{\omega_b^2}{\gamma^3(\omega - K_n v)^2 - 3K_n^2 v_{thb}^2} - \frac{\omega_p^2}{\omega^2 - 3K_n^2 v_{thp}^2} \tag{6}$$

Here, $\omega_p = (\frac{n_p e^2}{m \varepsilon_0})^{1/2}$ is the plasma frequency, $\omega_b = (\frac{n_b e^2}{m \varepsilon_0})^{1/2}$ is the beam frequency, ω is the angular frequency of the electromagnetic wave, γ is the electron beam energy, $v_{thp} = \sqrt{\frac{KT_p}{m}}$ is the thermal velocity of the plasma, $v_{thb} = \sqrt{\frac{KT_b}{m}}$ is the thermal velocity of the beam, v is the velocity of the beam, T_b is the beam temperature, T_p is the plasma temperature and K is the Boltzmann constant.

Dispersion equation

In the above physical model, its Maxwell equations can be written as:

$$\nabla \times B = \frac{-i\omega}{c} \varepsilon \cdot E, \tag{7}$$

$$\nabla \times E = \frac{i\omega}{c} B, \tag{8}$$

$$\nabla \cdot B = 0, \tag{9}$$

$$\nabla \cdot D = 0. \tag{10}$$

Suppose that every variable can be regarded as:

$$A = Ae^{i(K_n z - \omega t)}. \tag{11}$$

From Eqs. (7) and (8), we can obtain:

$$\nabla \nabla \cdot E - \nabla^2 E = \frac{\omega^2}{c^2} \varepsilon \cdot E \tag{12}$$

$$\nabla^2 E_z - [\nabla(\nabla \cdot E)]_z + \frac{\omega^2}{c^2} \varepsilon_3 E_z = 0, \tag{13}$$

Now Substituting Eq. (6) into Eq. (13), we have:

$$\nabla^2 E_z - [\nabla(\nabla \cdot E)]_z + \frac{\omega^2}{c^2} \times \left(1 - \frac{\omega_b^2}{\gamma^3(\omega - K_n v)^2 - 3K_n^2 v_{thb}^2} - \frac{\omega_p^2}{\omega^2 - 3K_n^2 v_{thp}^2} \right) E_z = 0 \tag{14}$$

From Eq. (10), we have:

$$\nabla \cdot \varepsilon_3 E_z = 0. \tag{15}$$

Substituting Eq. (6) into Eq. (15), we obtain:

$$\nabla \cdot E_z = \frac{\partial}{\partial z} E_z \left[\frac{\omega_b^2}{\gamma^3(\omega - K_n v)^2 - 3K_n^2 v_{thb}^2} + \frac{\omega_p^2}{\omega^2 - 3K_n^2 v_{thp}^2} \right]. \tag{16}$$

From Eqs. (13) and (16), the wave equation is obtained in the area of plasma beam as follows:

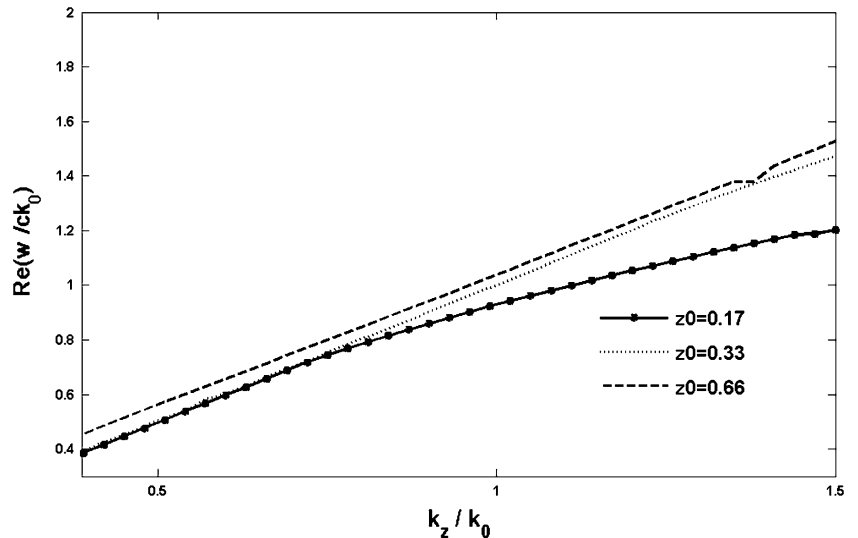
$$\left[\nabla_{\perp}^2 + \left(\frac{\omega^2}{c^2} - K_n^2 \right) \times \left(1 - \frac{\omega_b^2}{\gamma^3(\omega - K_n v)^2 - 3K_n^2 v_{thb}^2} - \frac{\omega_p^2}{\omega^2 - 3K_n^2 v_{thp}^2} \right) \right] E_z, \tag{17}$$

$$\nabla_{\perp}^2 = \nabla^2 - \frac{\partial^2}{\partial z^2}. \tag{18}$$

$$E_z(r, z) = E_{zn}(r) e^{i(K_n z - \omega t)}, \tag{19}$$

$$E_r(r, z) = \frac{iK_n}{c^2 - K_n^2} e^{i(K_n z - \omega t)} \frac{dE_{zn}}{dr}. \tag{20}$$

Fig. 2 Variation of normalized frequency $\text{Re}\left(\frac{\omega}{ck_0}\right)$ with normalized wave number $\left(\frac{k_z}{k_0}\right)$ for several values of the corrugation period. The chosen parameters are as follows: $n_p = 3 \times 10^{11}$, $R_0 = 1.60$, $h = 0.7$ and $T_p = 30 \times 10^8$



We investigate a ground state ($n = 0$) to solve the equation. With substituting Eq. (19) into Eq. (17), we have:

$$E_{zn} = \begin{cases} A_0 J_0(T_1 r) & 0 \leq r \leq R_b; \\ B_0 J_0(T_2 r) + C_0 N_0(T_2 r) & R_b \leq r \leq R(z); \end{cases} \quad (21)$$

$$T_1^2 = \left(\frac{\omega^2}{c^2} - K_n^2\right) \times \left(1 - \frac{\omega_b^2}{\gamma^3(\omega - K_n v)^2 - 3K_n^2 v_{thb}^2} - \frac{\omega_p^2}{\omega^2 - 3K_n^2 v_{thp}^2}\right), \quad (22)$$

$$T_2^2 = \left(\frac{\omega^2}{c^2} - K_n^2\right) \left(1 - \frac{\omega_p^2}{\omega^2 - 3K_n^2 v_{thp}^2}\right). \quad (23)$$

The field components must satisfy the following continuity equations (first boundary condition):

$$E_z(r = R_b^-) = E_z(r = R_b^+), \quad (24)$$

$$E_r(r = R_b^-) = E_r(r = R_b^+). \quad (25)$$

As a result, the field components are obtained as follows:

$$B_0 = -\frac{\pi}{2} R_b s_0 A_0, \quad (26)$$

$$C_0 = -\frac{\pi}{2} R_b l_0 A_0, \quad (27)$$

where

$$s_0 = T_2 J_0(T_1 R_b) N_1(T_2 R_b) - T_1 J_1(T_1 R_b) N_0(T_2 R_b), \quad (28)$$

$$l_0 = T_1 J_0(T_2 R_b) J_1(T_1 R_b) - T_2 J_0(T_1 R_b) J_1(T_2 R_b). \quad (29)$$

At the perfectly conducting corrugated waveguide surface (Second boundary condition), the tangential electric field must be zero,

$$E_z(r = R(z)) + E_r(r = R(z)) \frac{dR(z)}{dz} = 0. \quad (30)$$

With substituting Eqs. (19), (20) and (21) into Eq. (30), we investigate second boundary condition in ground state ($n = 0$) to achieve the dispersion equation.

$$B_0 J_0(T_2 R(z)) + C_0 N_0(T_2 R(z)) e^{i(K_0 z - \omega t)} + \frac{iK_0}{\frac{\omega^2}{c^2} - K_0^2} e^{i(K_0 z - \omega t)} \times \frac{d}{dR(z)} [B_0 J_0(T_2 R(z)) + C_0 N_0(T_2 R(z)) e^{i(K_0 z - \omega t)}] \times \frac{dR(z)}{dz} = 0, \quad (31)$$

Using the factorization of Eq. (31) and substituting B_0 and C_0 , we obtain:

$$-e^{i(K_0 z - \omega t)} \frac{\pi}{2} R_b A_0 \left(1 + \frac{iK_0}{\frac{\omega^2}{c^2} - K_0^2} \frac{d}{dz}\right) \times [s_0 J_0(T_2 R(z)) + l_0 N_0(T_2 R(z))] = 0. \quad (32)$$

$$D \cdot A = D_n A_n = D_0 A_0 = 0, \quad (33)$$

“A” is a vector with element A_0 and “D” is a matrix with element D_0 . With the help of derivative of Bessel functions, the dispersion relation can be obtained as, [18–22]

$$D_0 = \left(1 + \frac{iK_0}{\frac{\omega^2}{c^2} - K_0^2}\right) \times [T_2 h \kappa_0 (s_0 J_1 \sin(\kappa_0 z) + l_0 N_1 \sin(\kappa_0 z))] \quad (34)$$

Numerical result and discussion

The analysis of the dispersion relation is obtained by Eq. 34. First, we consider the dispersion analysis in the absence of the electron beam.

Fig. 3 Variation of normalized frequency $\text{Re}\left(\frac{\omega}{ck_0}\right)$ with normalized wave number $\left(\frac{k_z}{k_0}\right)$ for several values of the plasma temperature. The chosen parameters are as follows: $n_p = 3 \times 10^{11}$, $R_0 = 1.60$, $h = 0.7$, $R_b = 0.7$, $z = 0.33$ and $z_0 = 0.66$

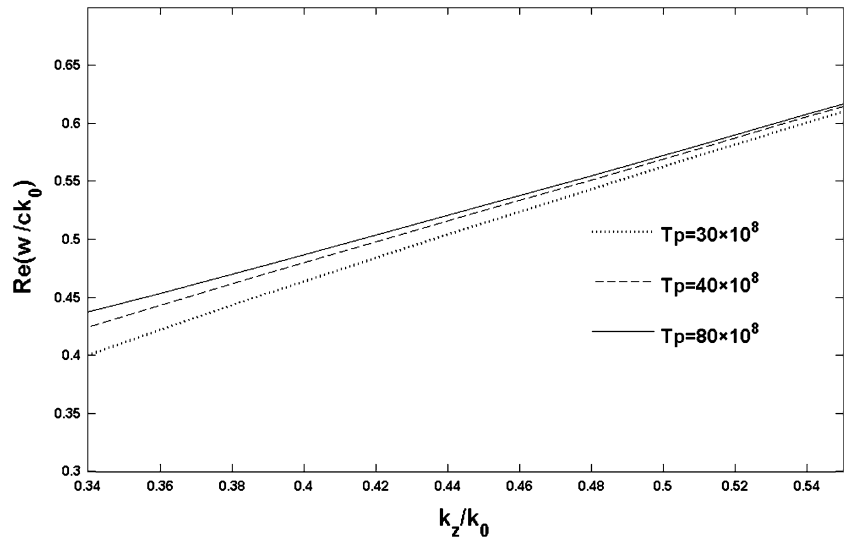


Fig. 4 Variation of normalized frequency $\text{Re}\left(\frac{\omega}{ck_0}\right)$ with normalized wave number $\left(\frac{k_z}{k_0}\right)$ for several values of the waveguide radius. The chosen parameters are as follows: $n_p = 3 \times 10^{11}$, $h = 0.7$, $R_b = 0.7$, $z = 0.33$, $T_p = 30 \times 10^8$ and $z_0 = 0.66$

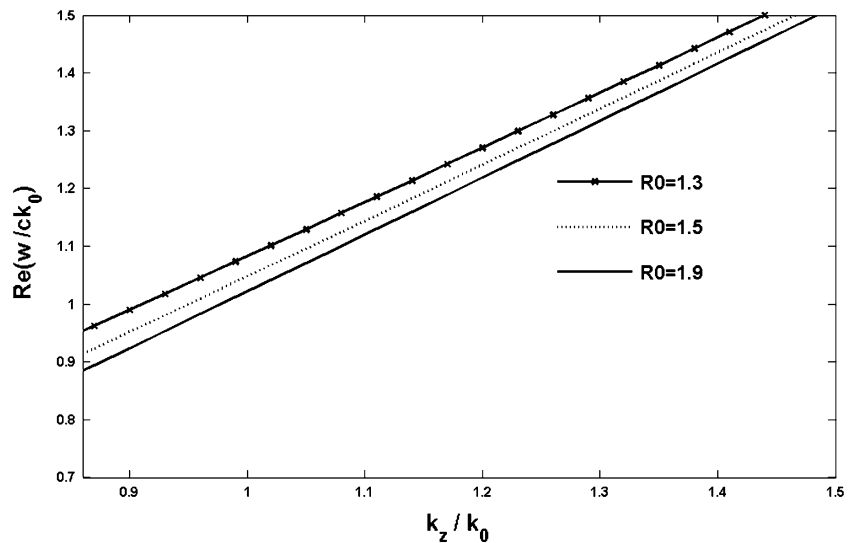


Fig. 5 Variation of normalized frequency $\text{Re}\left(\frac{\omega}{ck_0}\right)$ with normalized wave number $\left(\frac{k_z}{k_0}\right)$ for several values of the plasma density. The chosen parameters are as follows: $R_0 = 1.60$, $h = 0.7$, $R_b = 0.7$, $z = 0.33$, $z_0 = 0.66$ and $T_p = 30 \times 10^8$

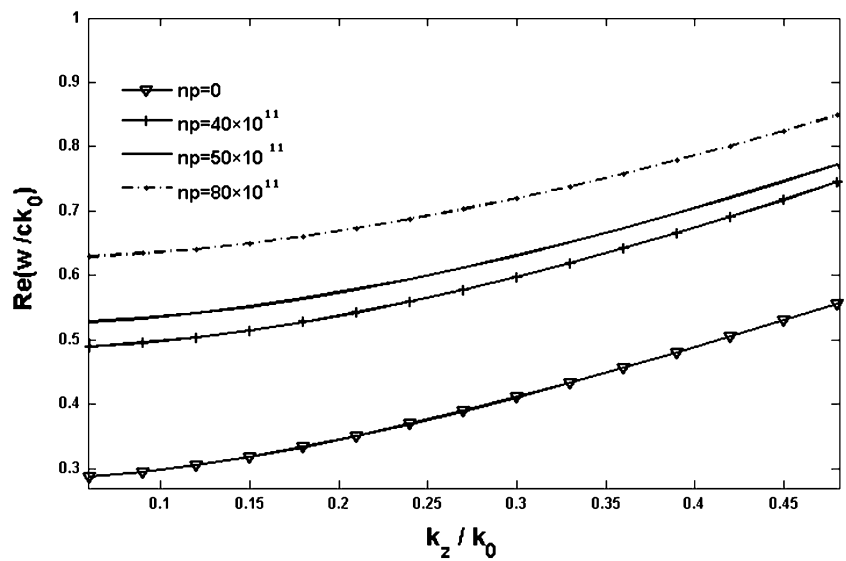


Fig. 6 Variation of the normalized growth rate $\text{Im}\left(\frac{\omega}{ck_0}\right)$ with normalized wave number $\left(\frac{k_z}{k_0}\right)$ for several values of the corrugation period. The chosen parameters are as follows: $\gamma = 1.001, h = 0.7, R_0 = 1.6, R_b = 0.7, z = 0.33, n_b = 10 \times 10^{11}, n_p = 3 \times 10^{11}, T_p = 30 \times 10^8$ and $T_b = 20 \times 10^7$

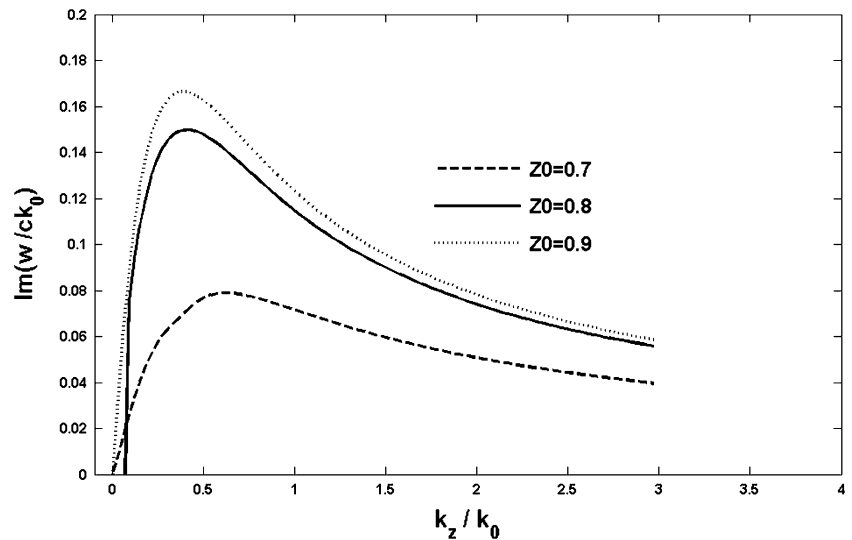


Fig. 7 Variation of the normalized growth rate $\text{Im}\left(\frac{\omega}{ck_0}\right)$ with normalized wave number $\left(\frac{k_z}{k_0}\right)$ for several values of the plasma temperature. The chosen parameters are as follows: $n_p = 3 \times 10^{11}, h = 0.7, R_0 = 1.6, z = 0.33, \gamma = 1.001, z_0 = 0.66, n_b = 10 \times 10^{11}$ and $T_b = 20 \times 10^7$

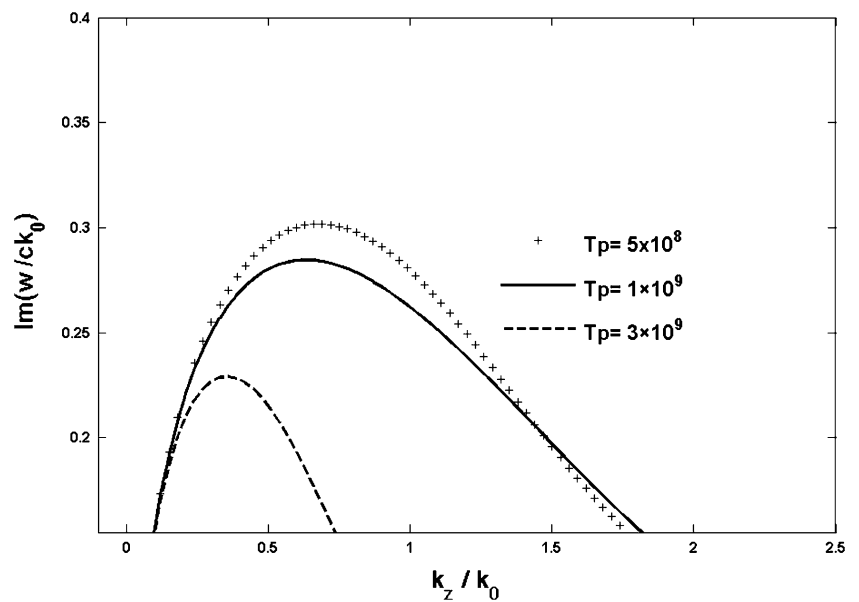


Figure 2 shows the variation of normalized frequency $\text{Re}\left(\frac{\omega}{ck_0}\right)$ versus wave number $\left(\frac{k_z}{k_0}\right)$ for several values of the corrugation period (z_0). As seen in this figure the effect of z_0 is to increase the frequency.

The effect of the plasma temperature on the frequency of the system as a function of k_z is shown in Fig. 3. This figure shows that the effect of plasma temperature increases the frequency. This effect is in good agreement with the thermal plasma dispersion relation $\omega^2 = \omega_p^2 + 3k_z^2 v_{th}^2$.

The effect of waveguide radius on the frequency of the wave as a function of k_z is shown in Fig. 4. As illustrated in this figure, the frequency decreases with increase in the waveguide radius. The phase velocity of the system

decreases by increasing the radius. It may be cause to the wave exit from the resonant condition.

Variations of the frequency as a function of the wave number for different values of the plasma density are shown in Fig. 5. It is clear that from the Fig. 5, the effect of plasma considerably increases the frequency. This effect is in good agreement with the simple relation of the plasma ($\omega^2 = \omega_p^2 + 3k_z^2 v_{th}^2$).

Now, we consider the analysis of the growth rate in the presence of the electron beam.

It is clear that from Fig. 6, the growth rate increases by increasing the corrugation period. The increase in the corrugation period helps the wave to be included in the resonant condition and finally increases the growth rate.

Fig. 8 Variation of the normalized growth rate $\text{Im}\left(\frac{\omega}{ck_0}\right)$ with normalized wave number $\left(\frac{k_z}{k_0}\right)$ for several values of the waveguide radius. The chosen parameters are as follows: $n_p = 3 \times 10^{11}$, $h = 0.7$, $T_p = 30 \times 10^8$, $R_b = 0.7$, $z = 0.33$, $\gamma = 1.001$, $z_0 = 0.66$, $n_b = 10 \times 10^{11}$ and $T_b = 20 \times 10^7$

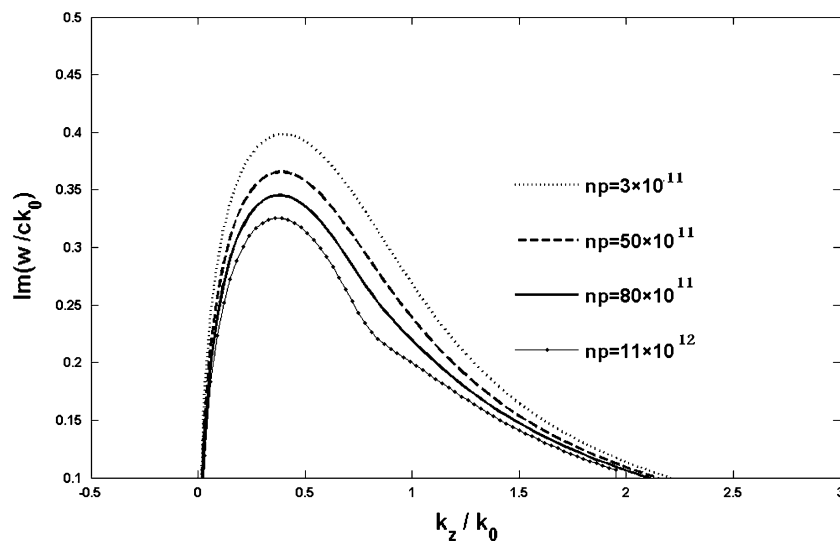
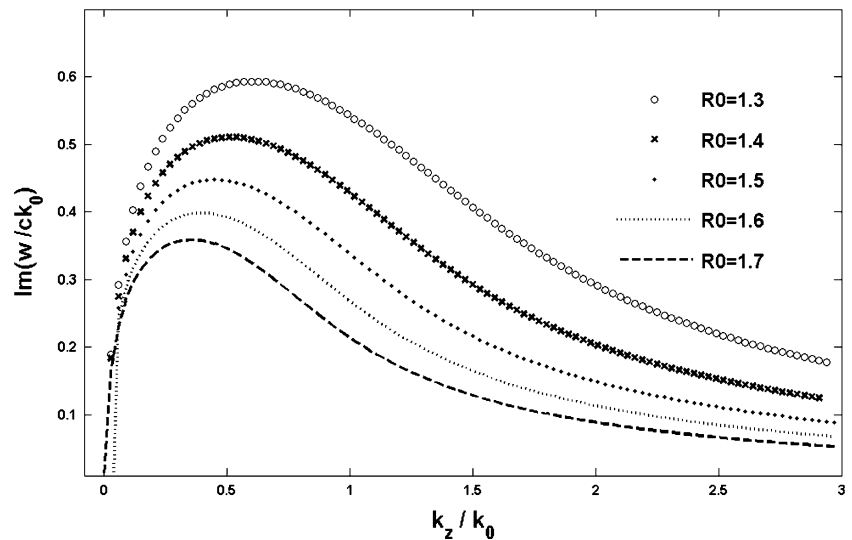


Fig. 9 Variation of the normalized growth rate $\text{Im}\left(\frac{\omega}{ck_0}\right)$ with normalized wave number $\left(\frac{k_z}{k_0}\right)$ for several values of the plasma density. The chosen parameters are as follows: $R_0 = 1.6$, $h = 0.7$, $T_p = 30 \times 10^8$, $R_b = 0.7$, $z = 0.33$, $\gamma = 1.001$, $z_0 = 0.66$, $n_b = 10 \times 10^{11}$ and $T_b = 20 \times 10^7$

It is clear that from Fig. 7, the plasma temperature considerably decreases the growth rate. By increasing the plasma temperature, the electrons exit from the resonant condition and finally decrease the growth rate.

As seen in Fig. 8, the growth rate decreases by increasing the R_0 . The waveguide radius has the important role in the determination of wave phase velocity. According to the Fig. 4, the phase velocity decreases by increasing the radius, and as seen in Fig. 8 the growth rate decreases by increasing the radius. By decreasing the phase velocity the wave exits from resonant condition.

The effect of the plasma density on the growth rate of the system as a function of the wave number is shown in Fig. 9. It is clear that in this frequency range the effect of plasma density is to decrease the growth rate of the system. According to the Fig. 5, the phase velocity increases by increasing the plasma density. By increasing the plasma density the wave exits from the resonant condition and finally the growth rate decreases.

It is clear that from Fig. 10, because of bunching effect, the increasing e-beam density increases the growth rate. As seen from Fig. 11, because of the synchronism condition, the effect of electron beam energy is to decrease the growth rate.

Fig. 10 Variation of the normalized growth rate $\text{Im}\left(\frac{\omega}{ck_0}\right)$ with normalized wave number $\left(\frac{k_z}{k_0}\right)$ for several values of the electron beam density. The chosen parameters are as follows: $R_0 = 1.6, h = 0.7, z = 0.33,$
 $R_b = 0.7, \gamma = 1.001, z_0 = 0.66, n_p = 3 \times 10^{11}, T_b = 20 \times 10^7$ and $T_p = 30 \times 10^8$

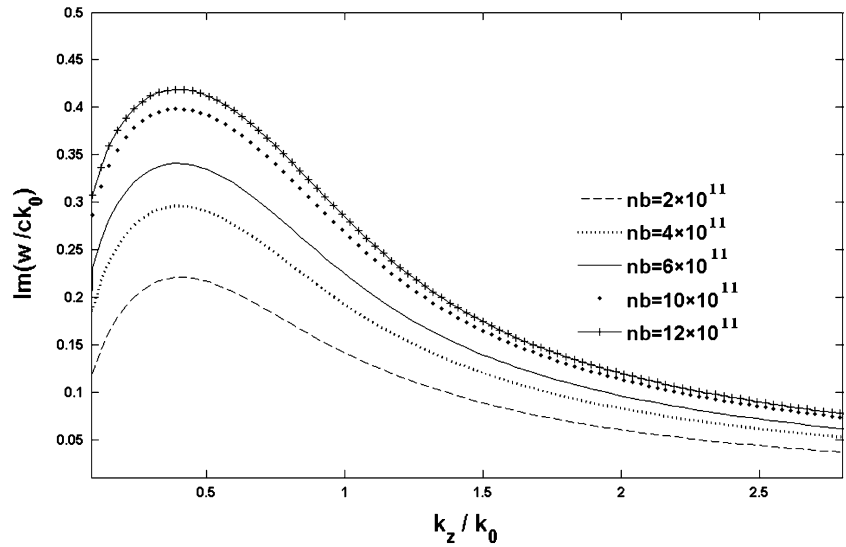
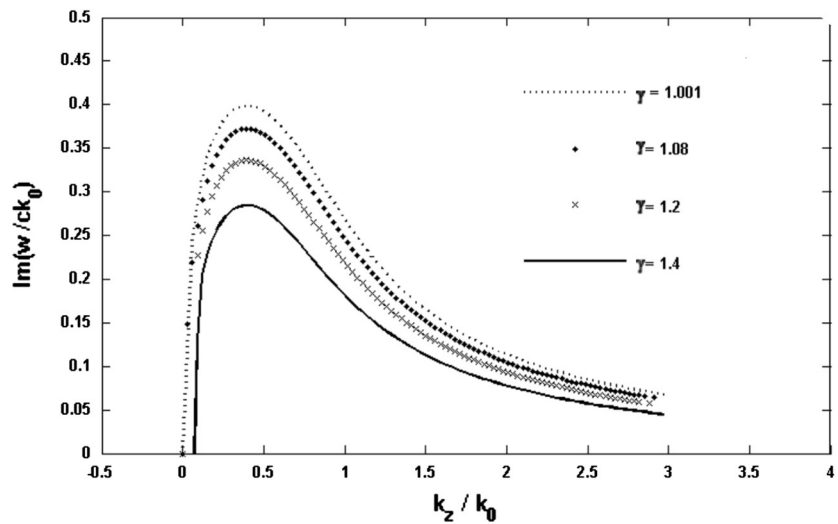


Fig. 11 Variation of the normalized growth rate $\text{Im}\left(\frac{\omega}{ck_0}\right)$ with normalized wave number $\left(\frac{k_z}{k_0}\right)$ for several values of the electron beam energy. The chosen parameters are as follows: $R_0 = 1.6, h = 0.7, z_0 = 0.66, R_b = 0.7, z = 0.33, n_b = 10 \times 10^{11}, T_p = 30 \times 10^8,$
 $n_p = 3 \times 10^{11}$ and $T_b = 20 \times 10^7$



Conclusions

In this paper, useful results are obtained as:

1. In the absence of the electron beam, the frequency increases by increasing the length of the corrugation period, plasma temperature and plasma density.
2. The frequency decreases by increasing the waveguide radius in the absence of the electron beam.
3. In the presence of the electron beam, the increase in the corrugation period and e-beam density help the wave to be included in the resonant condition and finally increase the growth rate.
4. The growth rate decreases by increasing the plasma temperature, waveguide radius, plasma density and e-beam energy and decreases the phase velocity. By decreasing the phase velocity the wave exits from resonant condition.

Open Access This article is distributed under the terms of the Creative Commons Attribution License which permits any use, distribution, and reproduction in any medium, provided the original author(s) and the source are credited.

References

1. Shiffler, D., Nation, J.A., Graham, S.K.: A high-power, traveling wave tube amplifier. *IEEE Trans. Plasma Sci.* **18**, 546 (1990)
2. Nusinovich, G.S., Carmel, Y., Antonsen, Jr.T.M.: *IEEE Trans. Plasm. Sci.* **26**, 628 (1998)
3. Kobayashi Jr, S., Antonsen, T.M., Nusinovich, G.S.: *IEEE Trans. Plasma Sci.* **26**, 669 (1998)
4. Pierce, J.R., Field, L.M.: *Traveling-wave tubes.* *Proc. IRE* **35**, 108 (1947)
5. Pierce, J.R.: *Travelling-Wave Tubes.* Van Nostrand Reinhold, New York (1950). (ch. 3)
6. Pierce, J.R.: *Theory of the beam-type traveling wave tube.* *Proc. IRE* **35**, 111 (1947)
7. Chu, L.J., Jackson, J.D.: *Proc. IRE* **36**, 853 (1948)

8. Freund, H.P., Ganguly, A.K.: Three-dimensional theory of the free electron laser in the collective regime. *Phys. Rev. A* **28**(6), 3438–3449 (1983)
9. Freund, H.P.: Multimode nonlinear analysis of free-electron laser, amplifiers in three dimensions. *Phys. Rev. A* **37**(9), 3371–3380 (1988)
10. Brillouin, L.: *Wave Propagation in Periodic Structures*. Dover, New York (1953)
11. Collin, R.E.: *Field Theory of Guided Waves*. McGraw-Hill, New York (1960)
12. Saviz, S.: The effect of beam and plasma parameters on the four modes of plasma-loaded traveling-wave tube with tape helix. *J. Theor. Appl. Phys.* **8**, 135 (2014)
13. Saviz, S., Salehizadeh, F.: Plasma effect in tape helix traveling-wave tube. *J. Theor. Appl. Phys.* **8**, 1 (2014)
14. Coaker, B., Challis, T.: Travelling wave tubes: modern devices and contemporary applications. *Microw. J.* **51**(10), 32 (2008)
15. Saviz, S., Shahi, F.: Analysis of axial electric field in thermal plasma-loaded helix traveling-wave tube with dielectric-loaded waveguide. *IEEE Trans. Plasma Sci.* **42**, 917 (2014)
16. Zavyalov, M.A., Mitin, L.A., Perevodchikov, V.I., Tskhai, V.N., Shapiro, A.L.: Powerful wideband amplifier based on hybrid plasma-cavity slow-wave structure. *IEEE Trans. Plasma Sci.* **22**, 600 (1994)
17. Saviz, S.: Plasma thermal effect on the growth rate of the helix traveling wave tube. *IEEE Trans. Plasma Sci.* **42**, 2023 (2014)
18. Miyamoto, K.: Parameter sensitivity of ITER type experimental tokamak reactor toward compactness. *J. Plasma Fusion Res.* **76**, 166 (2000)
19. Hong-Quan, X., Pu-Kun, L.: Theoretical analysis of a relativistic travelling wave tube filled with plasma. *Chin. Phys. Soc.* **16**(3), 766 (2007)
20. Chen, F.F.: *Introduction to Plasma Physics and Controlled Fusion*. Plenum Press, New York (1984)
21. Krall, N.A., Trivelpiece, A.W.: *Principles of Plasma Physics*. McGraw-Hill, New York (1973)
22. Goldston, R.J., Rutherford, P.H.: *Introduction to Plasma Physics*. Institute of Physics Publishing, London (1995)

