



Investigating the Failure Rate and Restoration Time of Medium Voltage Distribution Network to Use in Reliability Studies (Case Study)

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Article info	Abstract
<p>Keywords: Distribution Network, Reliability, Failure Rate, Restoration Time, Mean Time to Repair (MTTR)</p>	<p>Reliability studies in any system including electric distribution network require accurate estimation of the input parameters. Within the Iran's power distribution companies, the <i>event record</i> database encompasses locations and records of the network's power outages; these information subsequently will be used in dispatching affairs and emergencies of the distribution network. It should be noted that the historical data registered in the database might not be used directly for the analytical reliability studies. In such cases, data mining is required to acquire the useful information. This paper deals with methods of information extraction useful for reliability studies. The results of data mining in the Gilan Power Distribution Company (GPDC) along with comparison with the world references will be presented.</p>
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1. Introduction

The reliability is an important issue in various engineering fields and based upon the context, different approaches are used in order to quantitatively analyze it. According to [1], the reliability of a system is the probability of a system performing its purpose adequately for the period of time intended under the

operating conditions encountered. The power system is complex, highly integrated, and very large. Thus, its analysis as a whole system is overwhelming. Therefore, a hierarchical structure is defined for the reliability studies of the power systems in which the distribution networks are in the third level of the structure [2].

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The newest standard of the reliability for the distribution systems has introduced a variety of indices to analyze the electric distribution network reliability [3]. The standard proposes methods to separate the intense and scarce events which are studied within the resilience scope [4] from the usual and frequent ones considered for the reliability analysis. In order to calculate and analyze the reliability indices, it calls for simple and accurate analytical models or simulation-based modeling as Monte Carlo method, respectively studied in detail in [2], [5] and [6]. The input parameters to use these models are failure rate (λ) and restoration time (r) of the equipment.

In the Iran’s electric power distribution company, the power outages are registered in the *event record* database. However, these data cannot be used directly for the analytical reliability studies. In order to turn the registered data into useful ones, data mining is required. In [7-8] methods have been suggested to classify and refine the distribution network data. In this paper, in order to extract the useful information, steps of the so called data mining standard Cross-Industry Standard Process for Data Mining (CRISP-DM) will be adopted and implicitly presented in the next sections of the paper. The second part of the paper is dedicated to literature reviews. Finally, the summary and conclusions of the paper will be presented in the fifth section.

2- Literature Review

In the fourth chapter of [5], there are numerous information about reliability of devices based on historical data of companies, test data of producers, specialized organizations such as IEEE and CIGRE and technical journal and conference papers. Within the reference, there is no distinction between different overhead lines; however, three maximum and minimum values based on different and conventional researches are introduced for overhead lines and ground networks. The up and low figures, largest and lowest found mean values are in the published researches.

In [10], despite classifying the overhead lines into cross-armed (bare wire and covered conductors) and uncross-armed (Aerial Bundled and Spacer cables),

the failure rates of both classes are claimed to be the same. Thus, this only figure is adopted as enough for the overhead network. Within the same reference, there are, of course, distinctions between overhead lines and ground networks in one hand and urban and rural networks on the other.

In reliability analysis, it is customary as well as practical to measure the failure rate in terms of the length unit. In order to achieve this goal, tables of the mentioned references will be concluded as follows: 1) data registered in terms of the length unit are adopted without any changes; 2) failure rate of other data (assumed to be equal to the Gilan Power Distribution Company (GPDC) for the purpose of correct comparison) is multiplied by their frequency in a unit length; 3) results of the steps (1) and (2) are aggregated; 4) the unit length has been changed from mile into kilometer. The overall results of the studies are concluded in table 1.

Table 1: Conclusive Results of Failure Rates Data reported in [5] and [10]

Failure Rate in Ground Network (f/yr.km)	Failure Rate in Overhead Network (f/yr.km)	Studies Description
0.672	0.383	Maximum values in literatures [5]
0.104	0.126	Conventional Values in [5]
0.013	0.038	Minimum Values in [5]
0.063	0.172	Values for Urban Areas according to [10]
0.073	0.189	Values for Rural Areas according to [10]

The study of the network equipment restoration time is more intricate than that of the failure rate. Throughout the primary references [2], [5] and [10], in order to compute this time, such concepts as repair time and switching time or more accurately Mean-Time-To-Repair (MTTR) and Mean-Time-To-Switch (MTTS) have been used. In standard [11] values of repair time of equipment in the industrial areas are gathered. These values are too high and sporadic to be applicable to the electric distribution networks.

The more recent studies within the real distribution networks have shown that the restoration time (The

time interval from the moment power outage occurs until the moment service turns back) throughout the distribution networks is also of high dispersion, even though it is lower compared to the industrial areas. In [12] it has been shown that despite classification of various faults, the restoration time for each class again is highly dispersed, thus, choosing a typical representative for the whole data is practically impossible; there, researchers proposed using the log-normal distribution instead of a scalar value to represent the data; this method is typical and useful in approaches based upon repetition to some extent without applicability of the analytical methods. The proposal in [3] for separating the major event days from other days in order for reliability analysis is useful with respect to elimination of very large and sporadic events, however, as mentioned in [13-14], data of restoration time are still of very high dispersion and become even more intense in the presence of adverse weather conditions.

The more recent studies mostly present modeling patterns and in case of need for input parameters, they make use of previous researches summarized in [5] and [10]. The summary of the restoration times is given in table 2.

Table 2: Summary of the Restoration Times in [5] and [10]

Typical Restoration Time (hr.)	Maximum Restoration Times (hr.)	Minimum Restoration Times (hr.)	Studies Description
4	240	0.5	Reference [5]
2	24.5	-	Reference [10]

In [5], the minimum, typical and maximum values of restoration times are, respectively, 0.5, 4 (related to typical restoring of overhead line) and 240 (related restoration of Gas Insulated Substation) hours. In [10], the typical and maximum values of restoration times are reported to be, accordingly, 2 (associated with restoration of customers' service through replacing fuses) and 24.5 (associated with repairing the underground cable in rural areas) hours.

3- Failure Rate

Analysis of the power outages in [15] points out that over a 5-year time interval, the annual pattern of unscheduled power outages in the medium voltage networks are approximately similar as depicted in fig. 1.

If the momentary outages are eliminated and assuming that momentary break lead to operation of cut-out fuses which can be re-fused without any repair [16], the pattern of sustained power outages will be as in fig. 2.

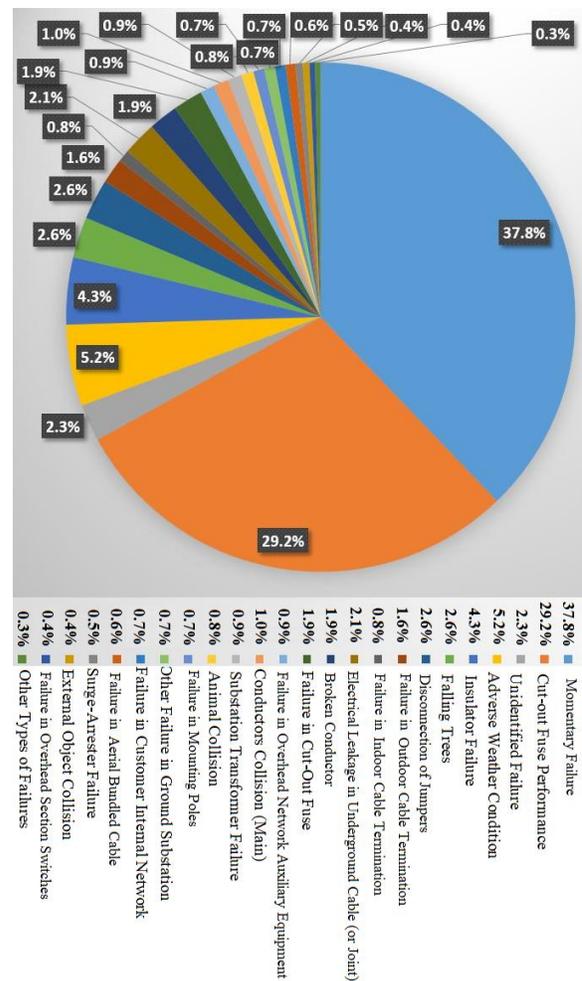


Fig. 1: Diagram of the Causes of Total Unscheduled Power Outages in GPDC [15]

[18], can be obtained through analysis of the data related to the scheduled emergency power interruptions registered in the event record database. This means a feeder based on a request from the repair crews is cut out, in order to emergently clear a fault to prevent occurrence of a bigger failure or spreading the power outage, with coordination of the dispatching control center and through a sub-transmission substation.

Fig. 4 illustrates details of time intervals related to scheduled emergency power interruptions which are registered in the event record database for various kind of reasons. The bar diagrams depict the minimum and maximum values of data, the box diagrams, the data between the first and third 4-quartiles and finally the rectangular diagrams, the mean values of the data.

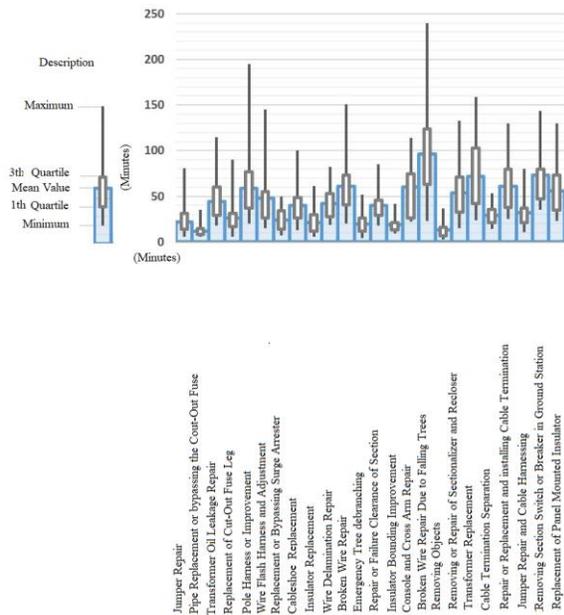


Fig. 4: Diagram of Pure Fault Clearance Time for each Type of Sustained Power Outages in Terms of #/min in GPDC [15]

In order to calculate the repair time, the sustained faults percentages shown in fig. 2 will be used as weighting coefficients to compute the weighted mean of the obtained times shown in fig. 4. In other words, given the number of each fault and its portion of the total faults along with the time for clearing each of them, value of mean Fault Clearance Time in each

section (subsection of a feeder) under study will be equal to the weighted mean of Fault Clearance Time of individual failures. The value of this weighted mean (mean Fault Clearance Time of each section) for the overhead lines and ground networks have been obtained, respectively, 30 and 41 minutes. These time can be used in simple models in which a set of elements constituting a section of feeder operates as a single element. It goes without saying that when wide-spreading and accurate models are adopted for reliability analysis, direct use of the results as depicted in fig. 4 will increase the accuracy of the study.

4-2 – Call-out (Dispatching) and Switching Time

The dispatching time implies the time interval needed for sending out the repair crews for investigating the faulted feeder up to the first maneuvering point/s and opening the related switch (or switches) and subsequently sending request for empowering feeder when no faulty section is found. Here, it has been assumed that there is always a standby repairmen who is not occupied with duties. The reason for such an assumption is priority of the medium voltage power outage over the low voltage, planning for adverse weather conditions and determining a watch list in the network operation departments. In cases where the repair teams are occupied, more complications will be involved which are addressed in [19-21].

Based on the definition given in this paper, this time can be determined using the data from multi-level restoration of unscheduled power outages registered in the event record database. The time of first registered maneuver in such power outages equals the dispatching time. The data of the database for GPDC spans from 10 up to 45 minutes with mean value equal to 20 minutes.

The switching time interval includes those needed to visit and going from the maneuver point n^{th} to the maneuver point $n + 1$, given that no failure is observed throughout the desired section (part of a feeder); this encompasses the time duration for opening the installed switch at the $(n + 1)^{th}$ and connecting the installed switch at the point n . These kind of data also can be extracted from the registered multi-level restoration of unscheduled power outage records in the

database. For the given case study of GPDC, these times span the interval 8 to 48 minutes with the mean value equal to 21 minutes.

4-3- Fault Identification Time

Determination of this time is more complicated than other times as there is no direct method to extract it from the registered data in the database. Reasonably, there are multitude of factors involved in the process. Type of the network (such as overhead Lines with covered or bare conductors, areial cables or ground network), time of day and night when failure occurs, types of failure, network observability from car road, the length of the line under investigation, and linemans’ skill are a few of these factors; thus, accurate determination of this time duration calls for a separate study involving in data mining and usage of machine learning algorithms such as neural network which cannot be fully covered in the current research. In this paper, a simple approach will be proposed which is matched to the power outage data.

In order to compute this time interval, the multi-level restoration of power outages are considered for two classes of feeders, first totally overhead and second totally ground network. Then the time interval between the last performed switching and ending the power outages are extracted. In this time interval, three different times are hidden: 1) fault identification time, 2) fault clearance time and 3) switching time to power back to the customers under power outage during failure. Therefore, through subtracting the clearance time and switching time calculated before from the total restoration time, logically must give the Fault Identification Time. This is done in table 4.

4 – 4 - Summary and Complementary Consideration of Restoration Time

In this paper, it has been suggested that the total restoration time is the sum of calling-out or dispatching time, necessary switching time, fault identification time and fault clearance time. In order to

achieve the minimum restoration time, the minimum registered times in each section must be taken into account. According to the previous sections, the minimum calling-out time is 10 minutes and that of the fault clearance time equals 3 minutes (related to minimum time needed to remove unwanted objects off the network). Assuming 2 minutes is needed for identification time, the total restoration time equals 15 minutes. This is the least required time to restore a given fault which led to a sustained power outage. Here, it has been assumed that there is no extra switching. Also, removing unwanted object off the network does not involve necessarily in securing the location and in some cases can be done remotely from the ground by the lineman.

Table 4: Estimation of the Sustained Fault Identification Time in GPDC [15]

Mean Identification Time per km (min/km)	Average Length of each Section (km)	Mean Identification Time in each Section (min/section)	Mean Fault Clearance Time (min)	Mean Switching Time (min/section)	Mean Restoration Time per Section (min/section)	Network Type
2.2	3.7	8	30	21	59	Overhead
2.3	1.3	3	41	21	65	ground

To determine the maximum restoration time, times for calling-out, fault identification, switching (considering 5 times switching with maximum 48 minutes for each switching) and fault clearance (related to maximum time required to repair broken conductor resulted from falling trees) are, respectively, considered to be 45, 30, 240 and 240 minutes. Also an extra 45 minutes time is considered for securing both sides of the faulty location; sum of these times, altogether, gives rise to 10 hours. This value here is the maximum theoretical time extracted from the studies. In practice, however, due to consistency of the distribution dispatching center, fast notification hierarchy and dispatching auxiliary repair crews, the restoration time is considerably lower than the maximum time. Exceptions to this are related to big storms, heavy snows and other disasters that

according to definition, must be studied in the system resilience scope.

In order to calculate the typical (average) restoration time, times for dispatch, fault identification, switching (considering 2 switching for which 21 minutes is required) and fault clearance are, respectively, taken to be 20, 8, 42, and 30 minutes. The sum of these time plus 20 minutes for securing the area equals 2 hours which is typical for clearing a multi-level power restoration.

It can be seen that there is a considerable difference between the results extracted here and those registered within the considered references. The most portion of this difference goes back, as explained in [11], to the way of defining the restoration time in different researches. Other factors can be related to repair crew dispatching or switching times, which are dependent upon the number of standby repair team against the extent of the area under consideration.

5- Conclusions

The input data are the main bases in analytical studies of reliability and researchers must not only consider the results of the global studies in his/her research. According to the findings of this paper, high level of failure in cable terminations and cable joints in GPDC is the main origin of highly unexpected failure rate (related to the reliability studies) of the aerial and ground cable network, which justifies the point just mentioned.

The high dispersion seen in restoration time of distribution power networks necessitates breaking down this time into smaller ones. This paper broke down the restoration time into times related to calling-out, network switching, fault identification and fault clearance; it also proposed solutions to determine each of these times given the facilities available to the Iran's electric distribution networks. Such a resolution in restoration time greatly help analytical studies related to reliability and would result in proposals and solutions to improve the non-complete automated distribution systems indices during the path to full-automated network.

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Table 3: Details of Reasons of Sustained Power Outage and Failure Rates of Medium Voltage Network Equipment in GPDC [15]

symbol	Failure Rate Caused by Failure in Overall Network (f/yr.km)	Mean Number of Equipment per km	Equipment Failure Rate (f/yr)	Total Number of Equipment in the Network	Total Length of The Effected Network	Type of Effected Network				Mean Annual Failure Rate	Type of Failure
						Ground	Overhead Line				
							Aerial Cable	Covered Conductor	Bare Wire		
λ_{unk}	0.019536	-	-	-	9674.6	*	*	*	*	189	Unidentified
λ_{whr}	0.050492	-	-	-	8239			*	*	416	Adverse Weather Condition
λ_{ins}	0.041615	83	0.000501	684111	8239			*	*	343	Failure in Insulator
λ_{tre}	0.025357	-	-	-	8202.9				*	208	Collision with trees
λ_{jmp}	0.024981	60.5	0.000413	498906	8239			*	*	206	Jumper Disconnection
λ_{oct}	0.127230	34.5	0.003688	34980	523.2		*			129	Failure in Outdoor Cable Termination
λ_{oct}	0.068225	18.5	0.003688	-	912.4	*					Failure in Outdoor Cable Termination
λ_{ict}	0.066636	17.7	0.003765	16203	912.4	*				61	Failure in Indoor Cable Termination
λ_{cbl}	0.189610	-	-	-	912.4	*				173	Electrical Leakage in Underground Cable (or Joints)
λ_{trg}	0.018206	-	-	-	8239			*	*	150	Broken Conductor
λ_{fcf}	0.019103	3.7	0.005163	29441	8762.2		*	*	*	152	Failures of Cut-Out Fuse

Table 3: Continued

λ_{pme}	0.008859	19.7	0.000450	162341	8239			*	*	73	Pole-Mounted Auxiliary equipment
λ_{con}	0.009346	–	–	–	8239			*	*	77	Conductors Collisions (or Bounding opening)
λ_{trs}	0.007433	2.6	0.002859	25185	9674.6	*	*	*	*	72	Substation Transformer Failure
λ_{anm}	0.007680	–	–	–	8202.9				*	63	Animal Collisions
λ_{pol}	0.006390	19.7	0.000324	172650	8762.2		*	*	*	56	Failure of mounted Poles
λ_{gsb}	0.060617	1.5	0.040411	1361	912.4	*				55	Other miscellaneous faults in Ground Substation
λ_{cst}	0.059185	–	–	–	912.4	*				54	Failure in Customer-side Network
λ_{ssb}	0.095566	–	–	–	523.2		*			50	Aerial Bundled Cable Failure
λ_{sga}	0.004239	9	0.000471	78564	8762.2		*	*	*	37	Surge Arrester Failure
λ_{obj}	0.004145	–	–	–	8202.9				*	34	External Objects Collisions
λ_{ssw}	0.003542	0.4	0.008855	3275	8762.2		*	*	*	29	Overhead Section Switches Failure (Except cutout fuses)
λ_{etc}	0.002894	–	–	–	9674.6	*	*	*	*	28	Other Types of Failures