

A Simplified Lagrangian Multiplier Approach for Fixed Head Short-Term Hydrothermal Scheduling

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Abstract. This paper presents a simplified lagrangian multiplier based algorithm to solve the fixed head hydrothermal scheduling problem. In fixed head hydrothermal scheduling problem, water discharge rate is modeled as quadratic function of hydropower generation and fuel cost is modeled as quadratic function of thermal power generation. The power output of each hydro unit varies with the rate of water discharged through the turbines. It is assumed that hydro plants alone are not sufficient to supply all the load demands during the scheduling horizon. In hydro scheduling, the specified total volume of water should be optimally discharged throughout the scheduling period. A novel mathematical approach has been developed to determine the optimal hydro and thermal power generation so as to minimize the fuel cost of thermal units. The performance of the proposed method is demonstrated with three test systems. The test results reveal that the developed method provides optimal solution which satisfies the various system constraints of fixed head hydrothermal scheduling problem.

Received: 18 July 2013; Revised: 23 October 2013; Accepted: 3 December 2013.

Keywords: hydrothermal scheduling, Lagrangian multiplier, fixed head, quadratic function.

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1. Introduction

The hydrothermal scheduling plays an important role in the operation planning of an interconnected power plant. The short-term hydrothermal scheduling problem is one of the most important daily activities for a utility company. Short-term hydrothermal scheduling

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involves the hour-by-hour scheduling of all generating units on a system to achieve minimum generation cost. The objective of fixed head hydrothermal scheduling is to minimize the fuel cost of thermal generating units by determining the optimal hydro and thermal generation schedule subject to satisfying water availability constraint and load demand in each interval of the scheduling horizon. The head of the reservoir is assumed to be constant for the hydro plants having reservoirs with large capacity. The hydraulic constraint imposed in the problem formulation is that the total volume of water discharged in the scheduling horizon must be exactly equal to the defined volume. The operational cost of hydroelectric units is insignificant because the source of hydro power is the natural water resources.

Numerous mathematical methods for the optimal resource allocation problems have been developed in the literature [6, 7]. Different mathematical methods for hydrothermal scheduling problem have been reported in the literature. In [12], an iterative technique based on computing LU factors of the Jacobian with partial pivoting for solving hydrothermal scheduling problem has been developed. A Lagrangian multiplier method for optimal scheduling of fixed head hydro and thermal plants is reported in [5]. This method linearizes the coordination equation and solves for the water availability constraint separately from unit generations. Dynamic programming approach [10] has been implemented for the solution of hydrothermal scheduling problem. The disadvantages of dynamic programming method are computational and dimensional requirements grow drastically with increase in system size and planning horizon. Lagrangian relaxation techniques have been proposed in the literature to solve hydrothermal coordination problem [11, 4]. A Lagrangian relaxation technique solves the dual problem of the original hydrothermal coordination problem. However the perturbation procedures are required to obtain primal feasible solution. These perturbation procedures may deteriorate the optimality of the solution obtained.

Recently, as an alternative to the conventional mathematical approaches, the heuristic optimization techniques such as simulated annealing [1], genetic algorithm [9], artificial immune algorithm [2] have been used to solve fixed head hydrothermal scheduling problem. Heuristic methods use stochastic techniques and include randomness in moving from one solution to the next solution. Due to the random search nature of the algorithm, these methods provide feasible optimal solution for the optimization problems. Neural network based approach has been developed for scheduling thermal plants in coordination with fixed head hydro units [3]. This method provides near-optimal solution for hydro thermal scheduling problem. An integrated technique of predator-prey optimization and Powell's method for optimal operation of hydrothermal system has been reported in [8]. In this hybrid method, predator-prey optimization is used as a base level search in the global search space and Powell's method as a local search technique.

In this paper, a new deterministic method based on Lagrangian multiplier and Newton method is developed for the solution of short-term fixed head hydrothermal scheduling problem. The scheduling period is divided into a number of subintervals each having a constant load demand. The proposed approach has been validated by applying it to three test systems.

2. Problem Formulation

The basic problem is to find the real power generation of committed hydro and thermal generating units in the system as a function of time over a finite time period from 1 to T. The goal is to minimize the total fuel cost required for the thermal generation in the scheduling period.

$$\text{Minimize } \varphi = \sum_{k=1}^T \sum_{i=1}^{NT} t_k F_{ik}(P_{Tik}) \quad (1)$$

where $F_{ik}(P_{Tik})$ is cost function of each thermal generating unit in interval k, which is

expressed by $F_{ik}(P_{Tik}) = a_i P_{Tik}^2 + b_i P_{Tik} + c_i$

T- number of periods for dividing the scheduling time horizon

NT- number of thermal generators

t_k - time in interval k

P_{Tik} - power generation level of ith thermal generating unit in interval k

a_i, b_i and c_i are the fuel cost coefficients of ith thermal generating unit

Subject to

(i) Power balance constraint

$$C_k = \sum_{i=1}^{NT} P_{Tik} + \sum_{i=1}^{NH} P_{Hik} - P_{Dk} = 0 \quad \text{for } k = 1, 2, \dots, T \quad (2)$$

where P_{Hik} - power generation level of ith hydro generating unit in interval k

P_{Dk} - Total generation demand in interval k.

NH - number of hydro generators

(ii) Water availability constraint

$$W_i = \sum_{k=1}^T t_k q_{ik}(P_{Hik}) = V_i - S_i \quad \text{for } i = 1, 2, \dots, NH \quad (3)$$

where q_{ik} is the discharge rate of hydro unit i during the kth interval, which is expressed

by $q_{ik}(P_{Hik}) = \alpha_i P_{Hik}^2 + \beta_i P_{Hik} + \delta_i$.

V_i is the pre-specified volume of water available for hydro unit i during the scheduling period. S_i is the total spillage discharge of ith hydro unit during the scheduling period and the spillage discharge is not used for power generation. α_i, β_i , and δ_i are the discharge coefficients of ith hydro unit with

$$P_{Ti}^{\min} \leq P_{Tik} \leq P_{Ti}^{\max} \quad (4)$$

$$P_{Hi}^{\min} \leq P_{Hik} \leq P_{Hi}^{\max} \quad (5)$$

where $P_{Ti}^{\min}, P_{Ti}^{\max}$ are the minimum and maximum generation limits of ith thermal unit and $P_{Hi}^{\min}, P_{Hi}^{\max}$ are the minimum and maximum generation limits of ith hydro unit.

3. Proposed Methodology

The Lagrangian equation for hydrothermal scheduling is

$$L(P, \lambda, \gamma) = \phi - \sum_{k=1}^T \lambda_k C_k + \sum_{i=1}^{NH} \gamma_i (W_i - (V_i - S_i)) \quad (6)$$

where λ_k is the Lagrangian multiplier for power balance constraint in kth interval and γ_i is the Lagrangian multiplier for hydro unit i. Substituting eqns. (1),(2) and (3) in eqn (6) gives

$$L(P, \lambda, \gamma) = \sum_{k=1}^T \sum_{i=1}^{NT} t_k F_{ik}(P_{Tik}) - \sum_{k=1}^T \lambda_k \left(\sum_{i=1}^{NT} P_{Tik} + \sum_{i=1}^{NH} P_{Hik} - P_{Dk} \right) + \sum_{i=1}^{NH} \gamma_i \left(\sum_{k=1}^T t_k q_{ik}(P_{Hik}) - (V_i - S_i) \right) \quad (7)$$

The minimum value is obtained by partially differentiating the Equation (7) with respect to $P_{Tik}, P_{Hik}, \lambda_k, \gamma_i$ and equating to zero

i.e $\frac{\partial L}{\partial P_{Tik}} = 0 \quad (8)$

i.e
$$t_k \frac{\partial F_{ik}(P_{Tik})}{\partial P_{Tik}} - \lambda_k \frac{\partial C_k}{\partial P_{Tik}} = 0 \tag{9}$$

Equation (9) gives

$$t_k(2a_i P_{Tik} + b_i) = \lambda_k \tag{10}$$

i.e
$$\frac{\partial L}{\partial P_{Hik}} = 0 \tag{11}$$

therefore
$$-\lambda_k + \gamma_i \frac{\partial}{\partial P_{Hik}}(W_i - (V_i - S_i)) = 0 \tag{12}$$

Equation (12) gives

$$t_k \gamma_i [2\alpha_i P_{Hik} + \beta_i] = \lambda_k \tag{13}$$

i.e
$$\frac{\partial L}{\partial \lambda_k} = 0 \tag{14}$$

therefore
$$C_k = 0 \tag{15}$$

Equation (15) gives

$$\sum_{i=1}^{NT} P_{Tik} + \sum_{i=1}^{NH} P_{Hik} = P_{Dk} \tag{16}$$

i.e
$$\frac{\partial L}{\partial \gamma_i} = 0 \tag{17}$$

therefore
$$W_i - (V_i - S_i) = 0 \tag{18}$$

Equation (18) gives

$$\sum_{k=1}^T t_k [\alpha_i P_{Hik}^2 + \beta_i P_{Hik} + \delta_i] = V_i - S_i \tag{19}$$

From the Equation (10), we get

$$P_{Tik} = \frac{\lambda_k - b_i}{2a_i} = \lambda_k \frac{1}{2a_i} - \frac{b_i}{2a_i}$$

$$P_{Tik} = \lambda_k A_i - B_i \text{ for } i = 1, 2, \dots, NT, k = 1, 2, \dots, T \tag{20}$$

where $A_i = \frac{1}{2a_i}$; $B_i = \frac{b_i}{2a_i}$

From the Equation (13), we get

$$P_{Hik} = \frac{\lambda_k - \beta_i \gamma_i}{2\alpha_i \gamma_i} = \frac{\lambda_k}{2\alpha_i \gamma_i} - \frac{\beta_i}{2\alpha_i}$$

$$P_{Hik} = \frac{\lambda_k}{\gamma_i} C_i - D_i \text{ for } i = 1, 2, \dots, NH, k = 1, 2, \dots, T \tag{21}$$

where $C_i = \frac{1}{2\alpha_i}$; $D_i = \frac{\beta_i}{2\alpha_i}$

Substituting Equations (20) and (21) in Equation (16) gives

$$\sum_{i=1}^{NT} (\lambda_k A_i - B_i) + \sum_{i=1}^{NH} \left(\frac{\lambda_k C_i}{\gamma_i} - D_i \right) = P_{Dk} \text{ for } k = 1, 2, \dots, T$$

therefore
$$\lambda_k = \frac{P_{Dk} + \sum_{i=1}^{NT} B_i + \sum_{i=1}^{NH} D_i}{\sum_{i=1}^{NT} A_i + \sum_{i=1}^{NH} \frac{C_i}{\gamma_i}} \text{ for } k = 1, 2, \dots, T \tag{22}$$

Substituting Equation (22) in Equation (21) gives

$$P_{Hik} = \frac{C_i}{\gamma_i} \left[\frac{P_{Dk} + \sum_{i=1}^{NT} B_i + \sum_{i=1}^{NH} D_i}{\sum_{i=1}^{NT} A_i + \sum_{i=1}^{NH} \frac{C_i}{\gamma_i}} \right] - D_i \tag{23}$$

for $i=1, 2, \dots, NH$, for $k=1, 2, \dots, T$

Substituting (23) in (19), we get

$$\sum_{k=1}^T t_k \left(\alpha_i \left[\frac{C_i}{\gamma_i} \left[\frac{P_{Dk} + \sum_{i=1}^{NT} B_i + \sum_{i=1}^{NH} D_i}{\sum_{i=1}^{NT} A_i + \sum_{i=1}^{NH} \frac{C_i}{\gamma_i}} \right] - D_i \right]^2 \right. \\ \left. + \beta_i \left[\frac{C_i}{\gamma_i} \left[\frac{P_{Dk} + \sum_{i=1}^{NT} B_i + \sum_{i=1}^{NH} D_i}{\sum_{i=1}^{NT} A_i + \sum_{i=1}^{NH} \frac{C_i}{\gamma_i}} \right] - D_i \right] + \delta_i \right) = V_i - S_i \tag{24}$$

for $i=1, 2, \dots, NH$

By expanding the Equation (24)

$$\sum_{k=1}^T t_k \left(\alpha_i \left[\frac{C_i^2}{\gamma_i^2} \left[\frac{P_{Dk} + \sum_{i=1}^{NT} B_i + \sum_{i=1}^{NH} D_i}{\sum_{i=1}^{NT} A_i + \sum_{i=1}^{NH} \frac{C_i}{\gamma_i}} \right]^2 + D_i^2 - \frac{2C_i D_i}{\gamma_i} \left[\frac{P_{Dk} + \sum_{i=1}^{NT} B_i + \sum_{i=1}^{NH} D_i}{\sum_{i=1}^{NT} A_i + \sum_{i=1}^{NH} \frac{C_i}{\gamma_i}} \right] \right] \right. \\ \left. + \beta_i \frac{C_i}{\gamma_i} \left[\frac{P_{Dk} + \sum_{i=1}^{NT} B_i + \sum_{i=1}^{NH} D_i}{\sum_{i=1}^{NT} A_i + \sum_{i=1}^{NH} \frac{C_i}{\gamma_i}} \right] - \beta_i D_i + \delta_i \right) = V_i - S_i \tag{25}$$

for $i=1, 2, \dots, NH$

Simplifying the Equation (25)

$$\frac{\alpha_i C_i^2}{\gamma_i^2} \sum_{k=1}^T \left[\frac{P_{Dk} + \sum_{i=1}^{NT} B_i + \sum_{i=1}^{NH} D_i}{\sum_{i=1}^{NT} A_i + \sum_{i=1}^{NH} \frac{C_i}{\gamma_i}} \right]^2 \\ + \left[\frac{\beta_i C_i}{\gamma_i} - \frac{2C_i D_i \alpha_i}{\gamma_i} \right] \left[\sum_{i=1}^{NT} A_i + \sum_{i=1}^{NH} \frac{C_i}{\gamma_i} \right] \sum_{k=1}^T \left[\frac{P_{Dk} + \sum_{i=1}^{NT} B_i + \sum_{i=1}^{NH} D_i}{\sum_{i=1}^{NT} A_i + \sum_{i=1}^{NH} \frac{C_i}{\gamma_i}} \right] \\ + \left[\sum_{i=1}^{NT} A_i + \sum_{i=1}^{NH} \frac{C_i}{\gamma_i} \right]^2 [24(\alpha_i D_i^2 - \beta_i D_i + \delta_i) - (V_i - S_i)] = 0 \tag{26}$$

for $i=1, 2, \dots, NH$

The Equation (26) is solved by Newton's method. The solution of these equations gives the values of $\gamma_1, \gamma_2, \dots, \gamma_n$. The detailed procedure for solving the simultaneous equations with two variables γ_1 and γ_2 by Newton's method is given below:

Let $f(\gamma_1, \gamma_2) = 0$, and $g(\gamma_1, \gamma_2) = 0$ (27)

Take γ_1^0 and γ_2^0 be the initial approximate solution for the above equation. The actual

solution is given by $(\gamma_1^0 + h)$ and $(\gamma_2^0 + m)$, where h is an incremental value of γ_1 and m is an incremental value of γ_2 .

$$\text{Therefore, } f(\gamma_1^0 + h, \gamma_2^0 + m) = 0 \tag{28}$$

$$g(\gamma_1^0 + h, \gamma_2^0 + m) = 0 \tag{29}$$

Expanding equations (28) and (29) by Taylor series,

$$f(\gamma_1^0, \gamma_2^0) + h \frac{\partial}{\partial \gamma_1} [f(\gamma_1^0, \gamma_2^0)] + m \frac{\partial}{\partial \gamma_2} [f(\gamma_1^0, \gamma_2^0)] = 0 \tag{30}$$

$$g(\gamma_1^0, \gamma_2^0) + h \frac{\partial}{\partial \gamma_1} [g(\gamma_1^0, \gamma_2^0)] + m \frac{\partial}{\partial \gamma_2} [g(\gamma_1^0, \gamma_2^0)] = 0 \tag{31}$$

Equations (30) and (31) can be written as

$$f_0 + h(f_{\gamma_1})_0 + m(f_{\gamma_2})_0 = 0 \tag{32}$$

$$g_0 + h(g_{\gamma_1})_0 + m(g_{\gamma_2})_0 = 0 \tag{33}$$

Equations (32) and (33) are solved for h and m using determinants,

$$\text{i.e } h = \frac{-D_{\gamma_1}}{D} \text{ and } m = \frac{-D_{\gamma_2}}{D} \tag{34}$$

$$\text{where } D = \begin{vmatrix} (f_{\gamma_1})_0 & (f_{\gamma_2})_0 \\ (g_{\gamma_1})_0 & (g_{\gamma_2})_0 \end{vmatrix}; \quad D_{\gamma_1} = \begin{vmatrix} f_0 & (f_{\gamma_2})_0 \\ g_0 & (g_{\gamma_2})_0 \end{vmatrix}; \quad D_{\gamma_2} = \begin{vmatrix} (f_{\gamma_1})_0 & f_0 \\ (g_{\gamma_1})_0 & g_0 \end{vmatrix}$$

By using the incremental values, the new values of γ_1 and γ_2 are obtained by

$$\gamma_1^{\text{new}} = \gamma_1^0 + h; \quad \gamma_2^{\text{new}} = \gamma_2^0 + m \tag{35}$$

Now γ_1^{new} and γ_2^{new} are taken as initial values and above process is repeated till the convergence criterion is satisfied.

The computational procedure for implementing the proposed method for the solution of fixed head hydrothermal scheduling problem is given in the following steps:

Step 1: Calculate the initial generation of thermal, hydro plants and initial λ_k from the following equations

$$P_{Tik} = \frac{P_{Dk}}{NT + NH} \quad \text{for } i = 1, 2, \dots, NT, k = 1, 2, \dots, T$$

$$P_{Hik} = \frac{P_{Dk}}{NT + NH} \quad \text{for } i = 1, 2, \dots, NH, k = 1, 2, \dots, T$$

$$\lambda_k = 2\alpha_i P_{Tik} + \beta_i \quad \text{for } i = 1, 2, \dots, NT, k = 1, 2, \dots, T$$

Step 2: Determine the initial values of γ_i^0 using Equation (13)

$$\text{i.e } \gamma_i^0 = \frac{\lambda_k}{2\alpha_i P_{Hik} + \beta_i} \quad \text{for } i = 1, 2, \dots, NH$$

Step 3: Substitute the values of γ_i^0 in Equation (26).

Step 4: Calculate the incremental values of γ_i using Equation (34).

Step 5: Calculate the new γ_i values using Equation (35).

Step 6: Substitute the new γ_i values in Equation (26) and then go to Step 4. This iterative procedure is continued till the difference between two consecutive iterations is less than specified tolerance.

Step 7: Calculate λ_k values from the Equation (22) by substituting the optimal values of γ_i .

Step 8: Determine the optimal generation schedule of thermal and hydro plants using eqns. (20) & (21).

4. Numerical Examples and Results

A mathematical approach developed in this paper has been implemented on three fixed head hydrothermal scheduling problems. The program is developed using MATLAB 7. The system data and results obtained through the proposed approach are given below

Table 1 Optimal generation schedule for Example 1

| Interval k | Demand P _{Dk} | Water discharge q _{1k} | Hydro generation P _{H1k} | Thermal generation P _{T1k} |
|------------|---------------------------|------------------------------------|--------------------------------------|--|
| 1 | 455 | 101.9329 | 234.2742 | 220.7258 |
| 2 | 425 | 101.0896 | 231.8794 | 193.1206 |
| 3 | 415 | 100.8105 | 231.0812 | 183.9188 |
| 4 | 407 | 100.5879 | 230.4426 | 176.5574 |
| 5 | 400 | 100.3937 | 229.8838 | 170.1162 |
| 6 | 420 | 100.9500 | 231.4803 | 188.5197 |
| 7 | 487 | 102.8422 | 236.8285 | 250.1715 |
| 8 | 604 | 106.2529 | 246.1679 | 357.8321 |
| 9 | 665 | 108.0848 | 251.0372 | 413.9628 |
| 10 | 675 | 108.3886 | 251.8354 | 423.1646 |
| 11 | 695 | 108.9992 | 253.4319 | 441.5681 |
| 12 | 705 | 109.3059 | 254.2301 | 450.7699 |
| 13 | 580 | 105.5423 | 244.2522 | 335.7478 |
| 14 | 605 | 106.2827 | 246.2477 | 358.7523 |
| 15 | 616 | 106.6104 | 247.1258 | 368.8742 |
| 16 | 653 | 107.7215 | 250.0793 | 402.9207 |
| 17 | 721 | 109.7988 | 255.5073 | 465.4927 |
| 18 | 740 | 110.3874 | 257.0240 | 482.9760 |
| 19 | 700 | 109.1524 | 253.8310 | 446.1690 |
| 20 | 678 | 108.4799 | 252.0749 | 425.9251 |
| 21 | 630 | 107.0292 | 248.2433 | 381.7567 |
| 22 | 585 | 105.6899 | 244.6513 | 340.3487 |
| 23 | 540 | 104.3705 | 241.0592 | 298.9408 |
| 24 | 503 | 103.3007 | 238.1057 | 264.8943 |

Problem- 1

$$\text{Minimize } F_1(P_{T1}) = \sum_{k=1}^{24} 0.001991 P_{T1k}^2 + 9.606 P_{T1k} + 373.7 \text{ dollars}$$

Subject to satisfying power demand in each interval and total water discharge during the entire scheduling horizon should be equal to the given water availability.

Total volume of water available for discharge (24 hours) V = 2559.6 M cubic ft

Water discharge $q_{1k}(P_{H1k}) = 0.0007749 P_{H1k}^2 - 0.009079 P_{H1k} + 61.53$ M cubic ft. per hour ;Total spillage S= 25.596 M cubic ft/24 hours

The optimal generation schedule obtained through the proposed method is given in Table 1. The solution converged in fifth iteration. The optimal value of $\gamma = 29.61852312$ and total amount of water utilized for hydro power generation exactly satisfied water availability constraint. The total fuel cost of thermal power generation is \$ 92097.74.

Problem- 2

$$\text{Minimize } F_1(P_{T1}) = \sum_{k=1}^{24} 0.01 P_{T1k}^2 + 3.0 P_{T1k} + 15 \text{ dollars}$$

Subject to satisfying power demand in each interval and total water discharge during the

entire scheduling horizon should be equal to the given water availability constraints.
 Total volume of water available for Hydro plant 1 (24 hours) $V_1 = 25$ M cubic ft
 Total volume of water available for Hydro plant 1 (24 hours) $V_2 = 35$ M cubic ft

Table 2 Optimal generation schedule for Example 2

| Interval k | Demand P_{Dk} | Water discharge | | Hydro generation | | Thermal generation P_{T1k} |
|---------------|--------------------|-----------------|----------|------------------|-----------|---------------------------------|
| | | q_{1k} | q_{2k} | P_{H1k} | P_{H2k} | |
| 1 | 30 | 0.7714 | 0.9543 | 18.4792 | 9.1003 | 2.4205 |
| 2 | 33 | 0.8105 | 1.0279 | 19.7041 | 10.2892 | 3.0067 |
| 3 | 35 | 0.8367 | 1.0772 | 20.5207 | 11.0817 | 3.3976 |
| 4 | 38 | 0.8760 | 1.1513 | 21.7456 | 12.2706 | 3.9838 |
| 5 | 40 | 0.9023 | 1.2009 | 22.5622 | 13.0631 | 4.3746 |
| 6 | 45 | 0.9684 | 1.3253 | 24.6038 | 15.0446 | 5.3517 |
| 7 | 50 | 1.0349 | 1.4505 | 26.6453 | 17.0260 | 6.3287 |
| 8 | 59 | 1.1556 | 1.6780 | 30.3201 | 20.5925 | 8.0874 |
| 9 | 61 | 1.1826 | 1.7288 | 31.1367 | 21.3851 | 8.4782 |
| 10 | 58 | 1.1421 | 1.6526 | 29.9118 | 20.1962 | 7.8920 |
| 11 | 56 | 1.1152 | 1.6019 | 29.0951 | 19.4037 | 7.5012 |
| 12 | 57 | 1.1286 | 1.6272 | 29.5034 | 19.7999 | 7.6966 |
| 13 | 60 | 1.1691 | 1.7034 | 30.7284 | 20.9888 | 8.2828 |
| 14 | 61 | 1.1826 | 1.7288 | 31.1367 | 21.3851 | 8.4782 |
| 15 | 65 | 1.2368 | 1.8310 | 32.7699 | 22.9702 | 9.2599 |
| 16 | 68 | 1.2776 | 1.9079 | 33.9948 | 24.1591 | 9.8461 |
| 17 | 71 | 1.3186 | 1.9851 | 35.2197 | 25.3479 | 10.4324 |
| 18 | 62 | 1.1961 | 1.7543 | 31.5450 | 21.7814 | 8.6737 |
| 19 | 55 | 1.1018 | 1.5766 | 28.6868 | 19.0074 | 7.3058 |
| 20 | 50 | 1.0349 | 1.4505 | 26.6453 | 17.0260 | 6.3287 |
| 21 | 43 | 0.9419 | 1.2754 | 23.7872 | 14.2520 | 4.9609 |
| 22 | 33 | 0.8105 | 1.0279 | 19.7041 | 10.2892 | 3.0067 |
| 23 | 31 | 0.7845 | 0.9788 | 18.8875 | 9.4966 | 2.6159 |
| 24 | 30 | 0.7714 | 0.9543 | 18.4792 | 9.1003 | 2.4205 |

Water discharge equations

$$q_{1k}(P_{H1k}) = 0.00005 P_{H1k}^2 + 0.03 P_{H1k} + 0.2 \text{ M cubic ft. per hour}$$

$$q_{2k}(P_{H2k}) = 0.0001 P_{H2k}^2 + 0.06 P_{H2k} + 0.4 \text{ M cubic ft. per hour}$$

Total spillage

$$S_1 = 0.25 \text{ M cubic ft/24 hours, } S_2 = 0.35 \text{ M cubic ft/24 hours}$$

The optimal generation schedule of hydro and thermal plants obtained through the proposed method is given in Table 2. The solution converged at fifth iteration. The optimal values of $\gamma_1 = 95.717727$ and $\gamma_2 = 49.311017$. The total fuel cost of thermal power generation is \$ 821.32.

Problem- 3

Minimize $F_1(P_{T1}) + F_2(P_{T2})$ where

$$F_1(P_{T1}) = \sum_{k=1}^{24} 0.0025 P_{T1k}^2 + 3.2 P_{T1k} + 25 \text{ dollars}$$

$$F_2(P_{T2}) = \sum_{k=1}^{24} 0.0008 P_{T2k}^2 + 3.4 P_{T2k} + 30 \text{ dollars}$$

Subject to satisfying power demand in each interval and total water discharge during the entire scheduling horizon should be equal to the given water availability constraints.
 Total volume of water available for Hydro plant 1 (24 hours) $V_1 = 2500$ M cubic ft
 Total volume of water available for Hydro plant 2 (24 hours) $V_2 = 2100$ M cubic ft

Table 3 Optimal generation schedule for Example 3

| Interval k | Demand P_{Dk} | Water discharge | | Hydro generation | | Thermal generation | |
|------------|-----------------|-----------------|----------|------------------|-----------|--------------------|-----------|
| | | q_{1k} | q_{2k} | P_{H1k} | P_{H2k} | P_{T1k} | P_{T2k} |
| 1 | 400 | 64.8580 | 21.3191 | 182.0811 | 32.6776 | 75.2100 | 110.0313 |
| 2 | 300 | 57.6834 | 9.5683 | 163.2297 | 13.9900 | 60.0679 | 62.7123 |
| 3 | 250 | 54.1537 | 3.7873 | 153.8040 | 4.6462 | 52.4969 | 39.0529 |
| 4 | 250 | 54.1537 | 3.7873 | 153.8040 | 4.6462 | 52.4969 | 39.0529 |
| 5 | 250 | 54.1537 | 3.7873 | 153.8040 | 4.6462 | 52.4969 | 39.0529 |
| 6 | 300 | 57.6834 | 9.5683 | 163.2297 | 13.9900 | 60.0679 | 62.7123 |
| 7 | 450 | 68.5029 | 27.2888 | 191.5068 | 42.0214 | 82.7810 | 133.6907 |
| 8 | 900 | 103.0338 | 83.8446 | 276.3381 | 126.1156 | 150.9203 | 346.6260 |
| 9 | 1230 | 130.3323 | 128.5549 | 338.5477 | 187.7847 | 200.8891 | 502.7785 |
| 10 | 1250 | 132.0405 | 131.3527 | 342.3180 | 191.5222 | 203.9175 | 512.2423 |
| 11 | 1350 | 140.6736 | 145.4921 | 361.1694 | 210.2098 | 219.0596 | 559.5612 |
| 12 | 1400 | 145.0477 | 152.6562 | 370.5951 | 219.5536 | 226.6306 | 583.2207 |
| 13 | 1200 | 127.7816 | 124.3772 | 332.8923 | 182.1784 | 196.3465 | 488.5828 |
| 14 | 1250 | 132.0405 | 131.3527 | 342.3180 | 191.5222 | 203.9175 | 512.2423 |
| 15 | 1250 | 132.0405 | 131.3527 | 342.3180 | 191.5222 | 203.9175 | 512.2423 |
| 16 | 1270 | 133.7549 | 134.1604 | 346.0883 | 195.2597 | 206.9459 | 521.7061 |
| 17 | 1350 | 140.6736 | 145.4921 | 361.1694 | 210.2098 | 219.0596 | 559.5612 |
| 18 | 1470 | 151.2359 | 162.7914 | 383.7911 | 232.6349 | 237.2301 | 616.3439 |
| 19 | 1330 | 138.9347 | 142.6441 | 357.3991 | 206.4723 | 216.0312 | 550.0974 |
| 20 | 1250 | 132.0405 | 131.3527 | 342.3180 | 191.5222 | 203.9175 | 512.2423 |
| 21 | 1170 | 125.2446 | 120.2221 | 327.2369 | 176.5721 | 191.8039 | 474.3871 |
| 22 | 1050 | 115.2350 | 103.8280 | 304.6152 | 154.1470 | 173.6334 | 417.6044 |
| 23 | 900 | 103.0338 | 83.8446 | 276.3381 | 126.1156 | 150.9203 | 346.6260 |
| 24 | 600 | 79.6677 | 45.5750 | 219.7839 | 70.0528 | 105.4941 | 204.6692 |

Water discharge equations

$$q_{1k}(P_{H1k}) = 0.000216 P_{H1k}^2 + 0.306 P_{H1k} + 1.98 \text{ M cubic ft. per hour}$$

$$q_{2k}(P_{H2k}) = 0.00036 P_{H2k}^2 + 0.612 P_{H2k} + 0.936 \text{ M cubic ft. per hour}$$

Total spillage

$$S_1 = 25 \text{ M cubic ft/24 hours, } S_2 = 21 \text{ M cubic ft/24 hours}$$

The optimal generation schedule of example 3 is given in Table 3. The solution converged at fifth iteration. The optimal values of $\gamma_1 = 9.2967$ and $\gamma_2 = 5.6269$. The total fuel cost of thermal power generation is \$ 47985.76.

5. Conclusion

A novel mathematical approach for the solution of fixed head hydrothermal scheduling problem is presented in this paper. The proposed method is implemented with test systems. The practical constraints of fixed head hydrothermal scheduling such as water availability constraints, waterspillage, power balance constraint in each interval and generation limits

of hydro and thermal units are taken into account in the problem formulation. Numerical results show that the proposed method has the ability to determine the global optimal solution and the method requires lesser number of iterations for the convergence.

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