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تحليل ميكروپلار پيزوترموالاستيسيته در يك سيلندر توخالی

مرجع پيزوالكتریک:

Steady-state thermal and mechanical stresses in Two-Dimensional Functionally Graded Piezoelectric Materials (2D-FGPMs) for a hollow in

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روابط کرنش-جابجایی:

$$\begin{aligned} \varepsilon_{rr} &= \frac{\partial u}{\partial r}, & \varepsilon_{\theta\theta} &= \frac{1}{r} \frac{\partial v}{\partial \theta} + \frac{u}{r}, \\ \varepsilon_{r\theta} &= \frac{1}{2} \left( \frac{1}{r} \frac{\partial u}{\partial \theta} + \frac{\partial v}{\partial r} - \frac{v}{r} \right), \\ E_r &= \frac{\partial \psi}{\partial r}, & E_\theta &= \frac{1}{r} \frac{\partial \psi}{\partial \theta}, \end{aligned} \quad (12)$$

where  $u$ ,  $v$ , and  $\psi$  are the displacement components, electric potential, and the radial and circumferential directions, respectively.

The asymmetric stress-strain and electric dis-

$$\begin{aligned} e_{rr} &= \frac{\partial u}{\partial r} \\ e_{\theta\theta} &= \frac{1}{r} \left( u + \frac{\partial v}{\partial \theta} \right) \\ e_{r\theta} &= \frac{\partial v}{\partial r} - \phi \\ e_{\theta r} &= \frac{1}{r} \left( \frac{\partial u}{\partial \theta} - v \right) + \phi \\ \chi_{rz} &= \frac{\partial \phi}{\partial r} \\ \chi_{\theta z} &= \frac{1}{r} \frac{\partial \phi}{\partial \theta} \end{aligned} \quad (1)$$

روابط خطی تنش- کرنش میکروپیلار ترموالاستیک بر اساس قانون هوک

The asymmetric stress-strain and electric displacement relations of FGPMs are as follows [11]:

$$\begin{aligned}
 \sigma_{rr} &= C_{11}\varepsilon_{rr} + C_{12}\varepsilon_{\theta\theta} + e_{21}E_r - C_1^T T(r, \theta), \\
 \sigma_{\theta\theta} &= C_{12}\varepsilon_{rr} + C_{22}\varepsilon_{\theta\theta} + e_{22}E_r - C_2^T T(r, \theta), \\
 \sigma_{zz} &= C_{12}(\varepsilon_{rr} + \varepsilon_{\theta\theta}) + e_{23}E_r - C_3^T T(r, \theta), \\
 \sigma_{r\theta} &= 2C_{44}\varepsilon_{r\theta} + e_{24}E_\theta, \\
 D_{rr} &= e_{21}\varepsilon_{rr} + e_{22}\varepsilon_{\theta\theta} - \varepsilon_{22}E_r + g_{21}T(r, \theta), \\
 D_{\theta\theta} &= 2e_{24}\varepsilon_{r\theta} - \varepsilon_{21}E_\theta + g_{22}T(r, \theta), \tag{13}
 \end{aligned}$$

$$\begin{aligned}
 \sigma_{rr} &= (2\mu + \lambda + \kappa)e_{rr} + \lambda e_{\theta\theta} \\
 \sigma_{\theta\theta} &= (2\mu + \lambda + \kappa)e_{\theta\theta} + \lambda e_{rr} \\
 \sigma_{r\theta} &= (\mu + \kappa)e_{r\theta} + \mu e_{\theta r} \\
 \sigma_{\theta r} &= (\mu + \kappa)e_{\theta r} + \mu e_{r\theta} \\
 m_{rz} &= \gamma\chi_{rz} \\
 m_{\theta z} &= \gamma\chi_{\theta z}
 \end{aligned} \tag{2}$$

که  $\lambda, \mu, \kappa, \gamma$  ثابت‌های میکروپیلار هستند همچنین در روابط فوق  $\sigma_{ij}(i, j = r, \theta)$  و  $m_{ij}(i, j = r, \theta, z)$  به ترتیب تنش نیرو و تانسور تنش کوپل می‌باشد.

معادلات تعادل میکروپلار الاستیسیته در مختصات استوانه‌ای دو بعدی  $(r, \theta)$

The stress and electric displacement equilibrium equations are written as follows:

$$\begin{aligned} \frac{\partial \sigma_{rr}}{\partial r} + \frac{1}{r} \cdot \frac{\partial \sigma_{r\theta}}{\partial \theta} + \frac{1}{r} (\sigma_{rr} - \sigma_{\theta\theta}) &= 0, \\ \frac{\partial \sigma_{r\theta}}{\partial r} + \frac{1}{r} \cdot \frac{\partial \sigma_{\theta\theta}}{\partial \theta} + \frac{2}{r} (\sigma_{r\theta}) &= 0, \\ \frac{\partial D_{rr}}{\partial r} + \frac{1}{r} \cdot \frac{\partial D_{\theta\theta}}{\partial \theta} + \frac{1}{r} (D_{rr}) &= 0. \end{aligned} \quad (15)$$

$$\begin{aligned} \frac{\partial \sigma_{rr}}{\partial r} + \frac{1}{r} \frac{\partial \sigma_{\theta r}}{\partial \theta} + \frac{\sigma_{rr} - \sigma_{\theta\theta}}{r} &= 0 \\ \frac{\partial \sigma_{r\theta}}{\partial r} + \frac{1}{r} \frac{\partial \sigma_{\theta\theta}}{\partial \theta} + \frac{\sigma_{\theta r} + \sigma_{r\theta}}{r} &= 0 \\ \frac{\partial m_{rz}}{\partial r} + \frac{1}{r} \frac{\partial m_{\theta z}}{\partial \theta} + \frac{m_{rz}}{r} + \sigma_{r\theta} - \sigma_{\theta r} &= 0 \end{aligned} \quad (3)$$

همچنین روابط سازگاری در مختصات قطبی به شکل زیر تعریف می‌شود [152]:

$$\begin{aligned} \frac{\partial e_{\theta r}}{\partial r} - \frac{1}{r} \frac{\partial e_r}{\partial \theta} + \frac{e_{\theta r} + e_{r\theta}}{r} - \frac{\partial \phi_z}{\partial r} &= 0 \\ \frac{\partial e_{\theta\theta}}{\partial r} - \frac{1}{r} \frac{\partial e_{r\theta}}{\partial \theta} + \frac{e_{\theta\theta} - e_{rr}}{r} - \frac{1}{r} \frac{\partial \phi_z}{\partial \theta} &= 0 \\ \frac{\partial m_{\theta z}}{\partial r} - \frac{1}{r} \frac{\partial m_{rz}}{\partial \theta} + \frac{m_{\theta z}}{r} &= 0 \end{aligned} \quad (104-3)$$