

ORIGINAL ARTICLE

Equilibrium and Kinetic Studies of Direct Red 81 Biosorption onto Modified Silk Maze as an Economical Biosorbent

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KEYWORDS

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ABSTRACT: In this study, the potential of biosorbent obtained from silk maze, was investigated for the batch biosorption of Direct red 81 (DR 81) in aqueous solution. The effects of temperature, biosorbent amount, contact time, initial dye concentration and ultrasonic irradiation were also evaluated. Furthermore, experimental equilibrium and kinetics data were fitted by Langmuir and Freundlich isotherms and pseudo-first-order and pseudo-second-order kinetic models, respectively. Kinetic experiments revealed that the biosorption of DR 81 onto modified silk maze can be described with a pseudo second-order model while the equilibrium isotherm data were well described by the Freundlich model. The negative thermodynamic values of ΔH° and ΔG° showed that the biosorption is an endothermic process and occurs spontaneously in the nature. The results presented that this waste material may be a suitable biosorbent for removal of industrial effluents due to its low cost and high efficiency.

INTRODUCTION

The huge rate in population growth has increased the demand for industrial products. Natural and synthetic dyes, as one of the main groups of organic pollutants, are extensively used in several industries involving textile, paper, printing and dye houses. The generation of these products leads to the formation of wastewater contaminated with dyes. The textile industry is responsible for the use of about 30% of synthetic dyes

[1]. Typical textile wastewater contains many types of dye molecules [2]. Many organic dyes are toxic to microorganisms and harmful to human beings. In the other hand, dye molecules have complex molecular of these products lead to the formation of wastewater contaminated with dyes. The textile industry is structures; they are very resistant to biodegradation [3, 5]. Hence, the treatment of effluents containing dyes has

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been a challenging problem among environmental technologies and it has always been necessary to find dye-removal efficient methods [6, 7]. Several methods have been reported for efficient removal of dyes from industrial wastewater, including, chemical precipitation [8], adsorption [9], electro-coagulation [10], biosorption [11, 12], electro-deposition [13] membrane systems [14], reverse osmosis and membrane filtration [15]. The conventional methods for treatment of the wastewater usually suffer from some disadvantages, including complicated procedures, formation of by-products, expensive and energy-intensive, limited versatility and less adaptability to a wide range of dye wastewaters [16]. Recently, there has been a growing interest in finding low-cost, easily obtainable, highly efficient, and environmentally benign alternatives to the current expensive methods [17, 18]. One of the biological processes is biosorption method. Biosorption may be simply defined as the removal of substances from solution by biological material. Such substances can be organic and inorganic. The biosorption process involves a solid phase (sorbent or biosorbent; biological material) and a liquid phase (solvent, normally water) containing a dissolved species to be sorbed (sorbate, dye molecules) [19, 20].

The major advantages of biosorption system for water pollution control are good removal performance, less investment in terms of initial cost, flexibility, simplicity of design, easiness of operation and insensitivity to toxic pollutants as compared with the conventional biological process treatment [21, 22]. Therefore, in the recent decades, there has been an increasing interest to find cheaper and easily provided natural adsorbents which are compatible with the environment. Certain natural materials such as banana pith [23], rice husk [24], papaya seeds [25], orange peel, banana peel [26], *Caulerparacemosa* var. *cylindracea* [27],

Caulerpalentillifera [28, 30], *Posidoniaoceanica* [31, 37], Camel Thorn Plant [38] and *Chamomilla* Plant [39] have been used for the treatment of wastewaters in previous studies. The present study aimed to present the usage of a natural environmental waste, silk maze, for the removal of dyes from industrial effluents. To obtain a better understanding of the biosorption mechanisms, the kinetic, isotherm and thermodynamic of dye removal were studied in batch system. Also, the effects of different parameters such as temperature, initial dye concentration, biosorbent dosage, contact time and ultrasonic irradiation were investigated on dye removal efficiency. Direct red was selected in this study as an azo-based dye model, which has been widely used in many industries.

MATERIALS AND METHODS

Materials

Direct red 81 ($C_{29}H_{19}N_5Na_2O_8S_2$) was purchased from Sigma–Aldrich Company, and was used without purification (Figure 1). Other chemical agents used were analytical-reagent grade and all the solutions were prepared with distilled water.

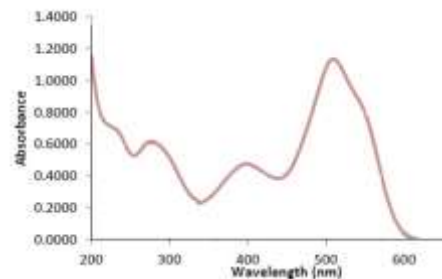
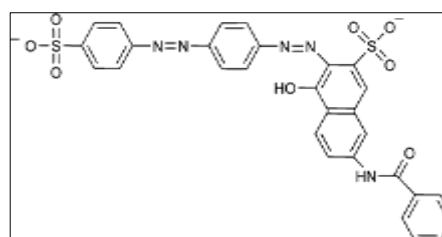


Figure1. The structure and UV Vis spectrum of DR 81

Preparation of biomass

The silk mazes were washed repeatedly with distilled water for removing dust, dried in an oven at 100°C and subsequently soaked in a H₃PO₄ solution for one day for protonation of biomass. Then, the biosorbent was filtered and heated until being dried. In the next step, the biosorbent was carbonized at 600°C for 20 minutes. The activated product was then cooled to room temperature. Finally, the dried biomass was ground and sieved to homogenous and fine small particles and stored in an air-tight polyethylene bottle.

Instrument

The residual DR 81 concentration was determined by using UV-Vis spectrophotometer (Perkin Elmer Lambda 25) at maximum wavelength of DR 81 (508 nm).

Batch experimental procedure

Batch biosorption experiments were performed on a mechanical stirrer using 500 mL beakers containing 250 mL of dye solutions. The influence of temperature, biosorbent dose, dye concentration and contact time, were optimized under the batch conditions. Kinetic studies at various temperatures of 25, 30, 35 and 40 °C under optimum conditions were conducted to verify the fitting of the experimental data to the first-order and the pseudo-second order kinetic models.

In order to analyze the biosorption equilibrium, we performed experiments changing initial dye concentration from 40 to 100 ppm. At the end of each experiment, the absorbances of the residual concentrations were measured by using the UV-Vis spectrophotometer.

Dye removal efficiency was computed through the following formula:

$$\% \text{Removal efficiency } \% = \frac{C_0 - C_f}{C_0} \times 100 \quad (1)$$

The amount of dye biosorbed onto unit weight of non-living sorbent, q_e (mg g⁻¹) was calculated using the mass balance equation given by:

$$q_e = (C_0 - C_f) \times \frac{V}{M} \quad (2)$$

Where q_e is the dye biosorption (mg g⁻¹), C_0 and C_f are the initial and equilibrium dye concentrations in the solution (ppm), respectively, V is the solution volume (L) and M is the biosorbent mass (g).

RESULTS AND DISCUSSION

The effect of contact time

The effect of contact time on the DR 81 removal by modified silk maze was studied by the variation of contact time from 10 to 70 min. for different initial dye concentrations of 40, 60, 80, 100 ppm with a biosorbent dosage equal to 1.5 g.

The effect of contact time on removal percentage of DR81 is shown in Figure 2. The results imply that the removal efficiency decreased from 97.7% to 60.3% with increase in the dye concentration from 40 to 100 ppm at the initial contact time of 30 min.

As can be seen, the contact time was an important parameter for the biosorption of the DR81 on modified silk maze. Subsequently, the removal efficiency of the DR81 reached to 97.7% and 95.2% at 70 min. for the initial dye concentrations of 40 and 100 ppm, respectively. A further increase in the contact time had a negligible effect on the efficiency of biosorption process. The adsorption of DR 81 on to modified silk maze was found to be rapid at initial period and then became slow and stagnated with increasing contact time (Figure 2). Thus, the dye adsorption by biosorbent was assumed to consist of three consecutive steps: (i) transport of adsorbate molecules from bulk solution to the exterior surface of adsorbent (film diffusion); (ii) transport of the adsorbate molecules within the pores of the adsorbent, which occurred on the external surface (intra-particle diffusion or pore diffusion); (iii) sorption of the adsorbate molecules on the interior surfaces of the pores and capillary spaces of the adsorbent [40]. Of the three steps, the third step was very rapid and could not be a rate-controlling step [41] and [42].

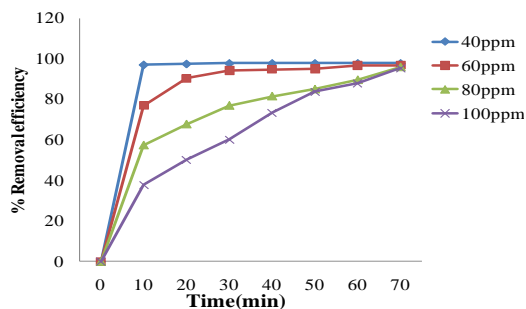


Figure 2. The effect of contact time on the DR81 removal by using 1.5 g modified silk maze (T=25°C)

In addition, Figure 3 shows dye biosorption at equilibrium (q_e) as well as the percent of removal efficiency over the range 40-100 ppm of initial concentrations.

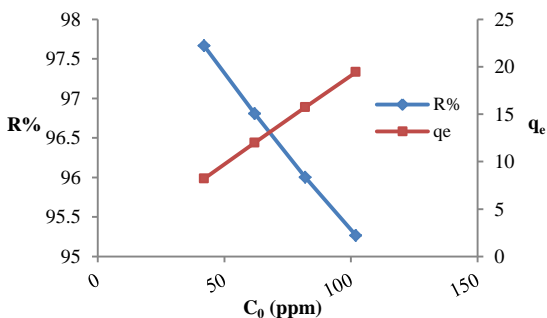


Figure 3. Biosorption plot at equilibrium (q_e) and removal efficiency percentage in different concentration

As can be seen, the dye removal efficiency decreased rapidly with increasing of initial concentration but q_e increased with increasing of initial concentration. In another part of this study, the kinetics data were analyzed using pseudo-first-order and pseudo-second-order kinetic models. The linear form of the pseudo-first-order rate equation can be defined as follows [43]:

$$\ln(q_e - q_t) = \ln q_e - k_1 t \quad (3)$$

Where q_e and q_t are the amounts of dye biosorbed at equilibrium and at time t (mg g^{-1}), and k_1 is the first-order rate constant (min^{-1}) for the biosorption. The

values of k_1 were calculated from the plot of $1/q_t$ versus $1/t$ (Figure 4).

The pseudo-second-order kinetic model expression [44] can be written as follows:

$$\frac{t}{q_t} = \frac{1}{(k_2 q_e^2)} + \frac{t}{q_e} \quad (4)$$

Where q_e and q_t are the amount of dye adsorbed at equilibrium and at time t , respectively (mg g^{-1}), and k_2 ($\text{g mg}^{-1} \text{min}^{-1}$) is the pseudo second-order rate constants. The values of k_2 were calculated from the plot of t/q_t versus t (Figure 5).

The linear regression coefficients close to 1 (Table 1) indicated that the biosorption of DR81 was fitted with the pseudo second order kinetics [45]. Also the Biosorption of Acid Orange 7 (AO7), C.I. Basic Red 46 (BR46) and C.I. Basic Blue 3 (BB3) dyes by green algal *Spirogyra* showed the similar results [46].

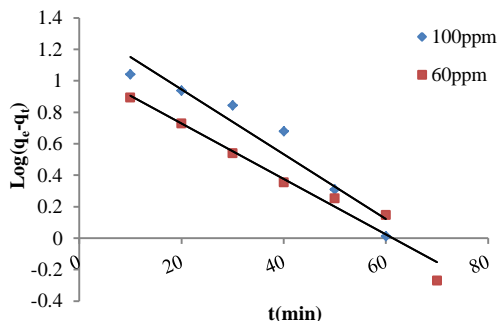


Figure 4. The pseudo first order kinetic plots for the biosorption of DR81 onto modified silk maze at different concentration (T=25°C)

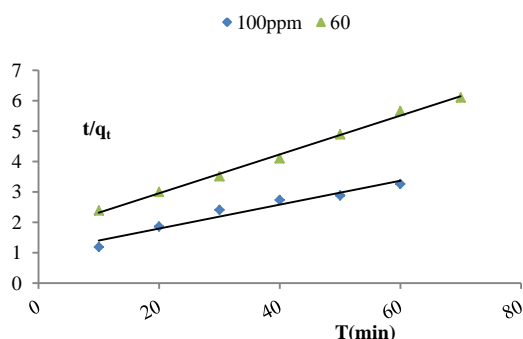


Figure 5. The pseudo second order kinetic plots for the biosorption of DR81 onto modified silk maze at different concentration (T=25°C)

Table 1. Kinetic parameters for biosorption of DR81 dye onto modified silk maze

Initial Concentration (ppm)	pseudo first order kinetic model		pseudo second order kinetic model	
	k_1 (min^{-1})	R^2	k_2 ($\text{g mg}^{-1} \text{min}^{-1}$)	R^2
60	4×10^{-2}	0.964	2.43×10^{-3}	0.996
100	4.7×10^{-2}	0.929	1.53×10^{-3}	0.993

The effect of biosorbent dosage

The effect of biosorbent dosage (1–2.5 g) was investigated on the biosorption of DR81 and the results are represented in Figure 6. As can be seen in this figure, dye removal efficiency increased rapidly with increasing of biosorbent until it reached the value of 98.9% having the biomass content of 2 g. The increase in the removal rate of DR81 can be explained by the increased surface area of the biosorbent and availability of more binding sites for dye molecules [47].

On the other hand, further increase in the biosorbent dosage up to 2 g did not significantly change the biosorption yield. This was due to the binding of almost all dye ions to biosorbent surface and the maintenance of equilibrium between the dye molecules on the biosorbent and those present in the solution [48, 49].

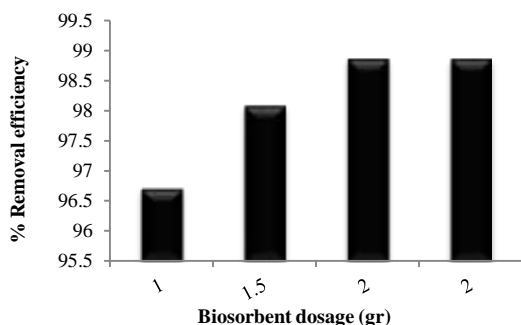


Figure 6. Effect of biosorbent dosage on removal efficiency of DR81 onto modified silk maze ($T = 25^\circ\text{C}$)

Biosorption isotherms

The results obtained from equilibrium isotherms were analyzed using Langmuir and Freundlich models. The Langmuir isotherm assumes a monolayer adsorption

onto a solid surface with a definite number of identical sites. It can be considered as Eq. (5): [50]

$$\frac{C_e}{q_e} = \frac{1}{q_{\max} K} + \frac{C_e}{q_{\max}} \quad (5)$$

Where q_e (mg g^{-1}) and C_e (mg L^{-1}) are the amount of biosorbed dye per unit mass of biosorbent and unadsorbed dye concentration in solution at equilibrium, respectively. q_{\max} is the maximum amount of the biosorbed dye per unit mass of biosorbent to form a complete monolayer on the surface bound at high C_e (mg g^{-1}), and K (L mg^{-1}) is a constant related to the affinity of the binding sites.

The Freundlich's adsorption isotherm model, which accounts for a multilayer heterogeneous adsorption, is widely used to describe the dyes biosorption isotherm. It is stated by exponential equation as Eq. (6): [51]

$$\ln(q) = \ln(K_f) + \frac{1}{n} \ln(C) \quad (6)$$

Where K_f (L g^{-1}) and $1/n$ are Freundlich isotherm constants related to biosorption capacity and intensity of biosorption, respectively. Figure 7 shows the linear plot of ($\log q_e$ versus $\log C_e$) of Freundlich isotherm.

The Langmuir and Freundlich constants and regression coefficients for the DR81 biosorption are collected in Table 2. Based on the R^2 values the Freundlich isotherm is better in predicting the DR81 biosorption than the Langmuir isotherm (Figure 7). It is noteworthy that the Freundlich constant $1/n$ smaller than unity indicated that the biosorption process was favorable under the optimal experimental conditions [52]. The biosorption of Acid Black 1 onto marine brown macroalgae showed same results [53].

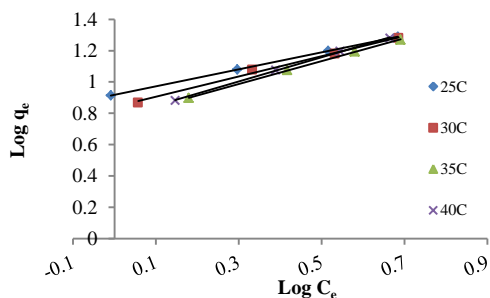


Figure 7. Freundlich isotherm plots for the biosorption of DR81 by modified silk maze at different temperatures

Table 2. Isotherm model parameters for the biosorption of DR81 onto modified silk maze.

T(K)	Freundlich isotherm			Langmuir isotherm		
	K _F	1/n	R ²	K _L	q _m	R ²
298	8.279	0.541	0.992	0.3548	30./30	0.985
303	6.934	0.646	0.993	0.2195	37.04	0.988
308	5.861	0.731	0.994	0.1304	47.62	0.983
313	5.902	0.772	0.989	0.1132	55.55	0.987

Thermodynamic studies

In order to describe the thermodynamic behavior of the biosorption of DR81 onto the modified silk maze, thermodynamic parameters were calculated including the change in free energy (ΔG^0), enthalpy (ΔH^0) and entropy (ΔS^0) from the following equations (Table 3) [54]:

$$\Delta G^0 = RT \ln K \quad (7)$$

$$\ln K = \frac{\Delta S^0}{R} - \frac{\Delta H^0}{RT} \quad (8)$$

Where R is the universal gas constant (8.314 J K⁻¹ mol⁻¹), T is the absolute temperature (Kelvin) and K represents the equilibrium biosorption constants of the

fitted isotherm. The values of ΔH^0 and ΔS^0 can be calculated from the slope and intercept of the linear plot of $\ln(K)$ versus $1/T$ (Figure 8).

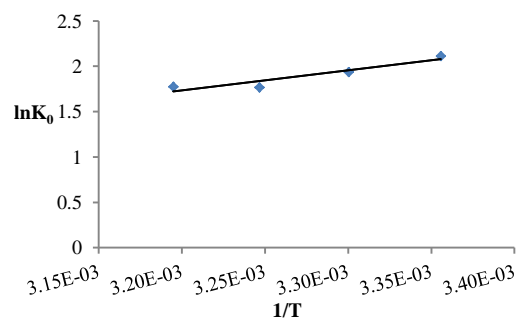


Figure 8. The plot of $\ln K$ versus $1/T$ for estimation of thermodynamic parameters for the biosorption of DR81 onto the modified silk maze.

Table 3. Thermodynamic parameters for biosorption of DR81 onto modified silk maze

T(K)	ΔG° (kJ/mol)	ΔH° (kJ/mol)	ΔS° (kJ/K mol)
298	-5.15		
303	-4.93		
308	-4.70	-18.44	-44.61
313	-4.48		

The negative values of ΔG° indicate that the DR81 biosorption onto modified silk maze was spontaneous and feasible at all the studied temperatures (25, 30, 35 and 40 °C). It was noted that the change in free energy for physical sorption was between -20 and 0 kJ mol^{-1} , but it was over the range -80 to -400 kJ mol^{-1} for the chemical sorption step. In addition, biosorption of DR 81 onto modified silk maze was a physical sorption process. Moreover, the negative value of ΔH° ($-9.74 \text{ kJ mol}^{-1}$) indicates that biosorption followed an exothermic process [55, 56]. The negative value of ΔS° also suggests decreased randomness at the solid/solution interface during the DR81 biosorption onto modified silk maze.

Effect of ultrasonic irradiations on biosorption of DR81 onto modified silk maze

The effect of ultrasonic irradiations on biosorption was studied by equipment operating at 40 kHz (DSA100-SK₂-4.0L). This biosorption experiment was performed by adding 1.5 g of biosorbent into a beaker containing 250 mL of initial concentrations 100 ppm of dye solution. These concentrations and biosorbent amount were selected because ultrasonic irradiation removed completely the DR81 in ten minutes with higher dose of biosorbent and lower concentration. Figure 9 indicates the effect of ultrasonic irradiations on the removal efficiency of DR 81 on to biosorbent. As can be seen, the removal efficiency increased with using the ultrasonic irradiations from 95.6% to 99.2% in 70 minutes. Moreover, the results show that removal efficiency was increased from 74.5% to 95.3% by using ultrasonic irradiation at the initial 30 minutes of contact time. This could be justified regarding the fact that at the presence of ultrasonic irradiations, there are more bubbles and

also the bubbles collapse more violently. This behavior can lead to more considerable effects on the biosorption process [57].

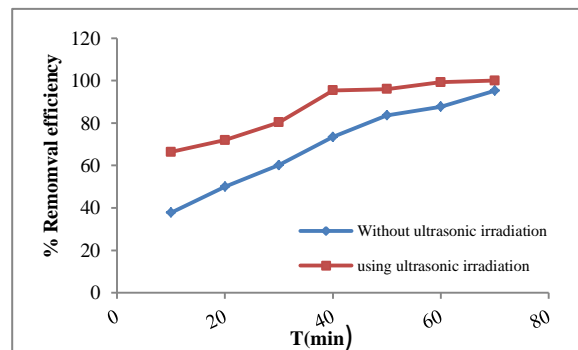


Figure 9. Effect of ultrasonic irradiations on removal efficiency of Direct red 81 on modified silk maze (dye concentration=100 ppm; biosorbent dosage= 1.5 g; T= 298K).

Activation energy

Arrhenius equation [58] was fitted by the use of pseudo-second-order rate constant to determine activation energy (E_a) for the biosorption of DR81 onto modified silk maze. The Arrhenius equation is expressed as:

$$\ln k = \ln A - \frac{E_a}{RT} \quad (9)$$

Where k is pseudo second order rate constant, A is the Arrhenius pre exponential factor or Arrhenius constant. The units of the pre-exponential factor A are identical to those of the rate constant and will vary depending on the order of the reaction and is the total number of collisions (leading to a reaction or not) per second, E_a is the activation energy (kJ mol^{-1}), R is the universal gas constant ($8.314 \text{ J mol}^{-1} \text{ K}^{-1}$), and T is the absolute temperature (K). The type of biosorption can be estimated by the magnitude of activation energy. Generally, low activation energies ($5\text{--}50 \text{ kJ mol}^{-1}$) are characteristics of physisorption, while higher activation

energies (60–800 kJ mol⁻¹) suggest chemisorption (chemical adsorption) [59]. Activation energy for the biosorption of DR81 onto modified silk maze was 48.24 kJ mol⁻¹, suggesting that the biosorption process could be mainly physisorption (physical biosorption) [60, 61].

CONCLUSION

In this study, the modified silk maze was used to biosorb DR81 from aqueous solution. The effects of different parameters such as temperature, biosorbent amount, contact time, initial dye concentration and ultrasonic irradiation were evaluated on removal efficiency. It was observed that the modified silk maze had maximum monolayer adsorption capacity, 55.5 mg/g. The Langmuir and Freundlich isotherms were well fitted with the experimental values. Based on the R² values the Freundlich isotherm is better in predicting the DR81 biosorption than the Langmuir isotherm.

The thermodynamic studies showed that the biosorption process was spontaneous and exothermic since the negative ΔG° value and negative ΔH° value. Also the biosorption of DR81 onto modified silk maze well agreed with the pseudo-second-order kinetic model (R² = 0.996). In addition activation energy for the biosorption of DR81 onto modified silk maze was 48.24 kJ mol⁻¹, suggesting that the biosorption process could be mainly physisorption. Also the effect of ultrasonic irradiations was studied on biosorption. The results showed removal efficiency increased with using the ultrasonic irradiations from 95.6% to 99.2% in 70 minutes

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