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# Examining the Mixing Plan and the Results of the Plastic Concrete

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# Abstract

In order to control seepage from the dam, various methods are used to reduce water seepage. One of the methods of reducing the permeability of the water according to its material is the formation of cut-off walls and filling them with plastic concrete materials. In this study, it has been tried to study the mixing plan of the plastic concrete of the main body of the cut-off wall of the Nargesi dam and to determine the relationships between results of different ages of compressive strength and elasticity modulus of 108 panels of cut-off wall in this project. The results indicate that the growth rate of elastic modulus in a period of time is less than the growth rate of the compressive strength, and in other words, the plasticity of the concrete is changed less over time. The results also show that the passage of time has a great influence on the compressive strength and modulus of elasticity and the passage of time, which is very effective in designing cutoff wall, significantly increases the compressive strength and modulus of elasticity. The relationship between the time parameter and the compressive strength is discussed in the present article.

Keywords: Compressive Strength, cut-off Wall, Elasticity Modulus, Empirical Relations, Plastic Concrete

# 1.Introduction

Dam construction projects may be essential in most countries due to the water crisis. One of the main and undoubtedly most important parts of this huge project is the cutoff walls. The inadequacy in cutoff walls construction and the lack of comprehensive information about the behavior of its components could cause the project to be destroyed or obsolete, given the high price it may cost.

Due to the abundant use of plastic concrete and its major application in the cut-off walls of the dam construction projects, plastic concrete has great importance. Studying a variety of the concrete's mixing plans and also modulus and determining the relationships between strength and process time seem necessary. Today, there are many articles on other types of concrete and civil engineers work with them, but plastic concrete, on the contrary to its high importance, is unknown for most engineers [1],[2].

This type of concrete has a very high strain and sensitivity which will have more complicated functions than conventional concrete. Considering the high cost of cut-off wall in dam construction in projects, if the plastic concrete is not prepared according to technical specifications, the dam may have cut-off problem and may be completely damaged or obsolete [1], [2].

Therefore, it is necessary to examine the topic in terms of making plastic concrete and its aspects, as well as in terms of recognizing the exact behavior of this concrete and its behavior over time. As there is usually a long time gap between the time of the construction of the walls and the exploitation stage, it is very important to estimate the strength relationships for the exploitation time.

Due to the flood phenomenon under the dams, in most cases underground water flows exist and water seepage affects the efficiency and proper function of the dam. The pressure of water and its outlet path through the dam foundation can be dangerous for dam's permanent installations. The excessive water seepage in the basement and dam body, in many cases, has resulted in damages to the earth dams. In all of the earth dams, the presence of water seepage is inevitable, but it is certain that proper cut-off methods should be used to minimize seepage to an acceptable level [3].

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The main application of the cut-off walls is for the underneath of the earth or pebble dam. Due to its high deformation, low permeability and proper compressive strength against forces, their use in loose soils, and saturated fine grains, cutoff method is often the most cost-effective method. Among the cut-off methods, the use of cut-off walls is very useful in alluvial foundations, and it can be said that the best cut-off option in these areas is the use of plastic concrete cut-off walls.

During concreting, bentonite slurry keeps gravel, sand and cement suspended in plastic concrete, which reduces the permeability during the setting time of concrete) and, according to the ICOLD proposal, a bentonite slurry is used to enhance the ductility of concrete [4]. The mixing plan of plastic concretes should have a permeability coefficient within the range of approximately  $10^{-7}$  to  $10^{-9}$  m / s and slump in the range of 15 to 22 cm. In general, bentonite is used in civil engineering sciences for cutoff purposes [5-13].

It should be noted that the use of plastic concrete cut-off walls under dams, in addition to adequate strength and durability against erosion, should have considerable ductility and flexibility to endure earthquake loading or burst load without cracking and losing cut-off attribute [1].

Kazemian et al. [14] studied the changes of various amounts of bentonite in plastic concrete and its physical properties. This study showed that as the bentonite increases, compressive strength and elasticity modulus are greatly reduced. In this research, to determine the elasticity modulus of plastic concrete by drawing a stress-strain diagram, according to ASTM D2166 standard, taking into account the gradient of the linear region of the graph, the relation  $E = (\sigma b - \sigma a) / (\varepsilon b - \varepsilon a)$  in which  $\sigma b$ is the maximum stress in the linear region of stressstrain curve,  $\sigma a$  is the minimum stress in linear stress-strain diagram, ɛb is the maximum strain in the linear region of stress-strain curve and *\varepsilon* as the minimum strain in the linear region of stress-strain curve, elasticity modulus.

Gholipour [15] studied the performance of plastic concrete in the implementation of cut-off dams (a case study of Karkhe Dam). In this research, plastic concrete of Karkheh Dam was studied using fusing iron slag. In this research, the permeability, single axial pressure and flexibility tests were performed on the samples. The results of the experiments showed that by increasing the consumption of slag up to 12.5%, the permeability of the samples decreased to about 80 times and with a consumption of 15% slag by 197 times. While the elasticity modulus increases significantly with the use of slag in the range of 10 to 12.5% cement weight.

Pashazadeh et al. [16] evaluated the design of a mixture of suitable plastic concrete with a composite method in separating walls to control the sediment under the earth dam. In their study, the use of concrete materials in the separator wall has traditionally attracted much attention due to its low permeability and high hydraulic gradients caused by underground drainage. The use of conventional concrete with a high elastic modulus may encounter problems such as wall imperfections, which occurs due to the dynamic pressure drop in the wall. To solve this problem, adding a certain percentage of clay (bentonite) to plastic concrete materials, reduces the hardness of concrete and also elasticity, which results in better flexibility and more. It has been shown that the addition of bentonite (clay and drilling mud) to plastic concrete materials reduces the risk of hydraulic fracturing and cracking.

Falaki [17] studied the mechanical properties of plastic concrete-containing bentonite using waste rubber powder. The purpose of this study was first to obtain the optimal amount of bentonite in the mixing plan of plastic concrete and then by the optimal mixing plan, obtaining the permissible percentage of replacement of waste rubber powder to the sand with maintaining proper mechanical properties. Further, consideration was given to the amount of changes in the mechanical properties of plastic concrete containing waste rubber for different percentages of this waste, which is a weight substitute for sand.

For this purpose, in the mixing plans of this study, waste from rubber powder in a size smaller than 1 mm and replacement of 3%, 7% and 10% weights by fine particles with different amounts of bentonite and water to cement ratio of 0.8 were compared with its mechanical properties with ordinary plastic concrete. To study the properties of plastic concrete, compressive strength, tensile strength, bending, elasticity modulus, water absorption, contraction, ultrasonic and electron microscopy tests were performed. The results indicated that by increasing the amount of rubber powder, a decrease in the compressive strength, flexural strength, tensile strength and elastic modulus of the plastic concrete would be seen. However, by increasing the amount of bentonite in the plastic concrete, one can partially control this negative effect and make concrete with similar properties to the original plastic concrete which contains waste rubber powder.

## **1.Evaluation of the Results of the Plastic Concrete of the Cut-Off Wall of the Main Body of Nargisi Dam**

#### 1.1.Nargesi Embankment Dam Site

The Nargesi embankment dam is located on Shirinrood River, approximately 45 km southeast of

Kazerun city in southwest of Iran (Fig. 1). The dam is categorized as an earth-fill embankment type with central impermeable clay core. The main goal of the dam is flood control, power generation and water supply. Fig. 2 shows view of Nargesi Dam and related structures.

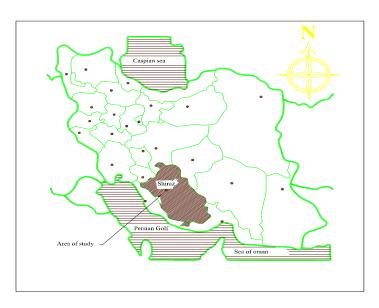


Fig. 1. Location Map of the Nargesi Dam Site

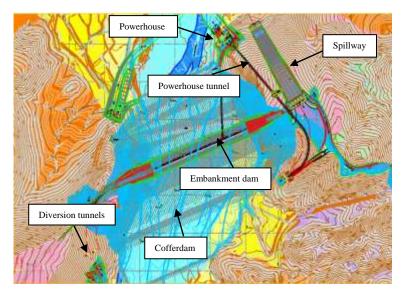


Fig. 2. View of Nargesi Embankment Dam and Related Structures.

The type of dam is limestone with clay core, the head of the river bed is 77.5 meters, the crest length is 600 meters, and the crest width is 10 meters. At the axis of this dam, the main body of the cut-off wall is drilled approximately 264 meters long and the average depth of 30 meters.

The method of drilling the cut-off wall of this project is discontinuous, in this way, the panels of the cutoff wall are drilled and run alternatively. In this method, the site of the cut-off wall is divided into S and P panels. Initially P panels are drilled and concreted, and after 28 days or after concrete's suitable initial set, P panels with drilling machine, S panels will be drilled and concreted by observing some suitable overlap. The width of the wall is different depending on the layout and size of the drilling device. In this project, the width of the wall

is 80 cm and the length of the panels is 2.4 meters. After complete drilling of the S and P panels, an entirely integrated wall was finally created. The view of the cutoff wall panels is shown in Fig. 3

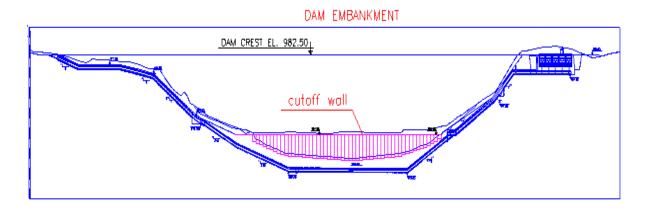


Fig. 3. Cross-Section of the Dam Body and Cutoff Wall

## 2.SPECIFICATIONS OF THE MATERIALS USED IN THE MIXING PLAN CONSUMABLES 2.1.Stone Materials

The used rock is a combination of broken and natural materials and is derived from the mines of the Shirin Roud River, which originates from the springs of Arjan plain. The specification of these materials is in accordance with Table 1.

Table 1

The distribution of specifications of the stone materials

| sand | Pea gravel | Almond gravel | Sieve number | (mm)Sieve size |
|------|------------|---------------|--------------|----------------|
| 100  | 100        | 100           | 1 1/2        | 38.1           |
| 100  | 100        | 100           | 1            | 25.4           |
| 100  | 100        | 93.3          | 3/4          | 19.05          |
| 100  | 100        | 22.22         | 1/2          | 12.7           |
| 99.7 | 73.6       | 2             | 3/8          | 9.52           |
| 99.2 | 1.8        | 0.5           | 4            | 4.76           |
| 80.4 | 0.1        | 0             | 8            | 2.36           |
| 60.1 | 0          | 0             | 16           | 1.18           |
| 34.8 | 0          | 0             | 30           | 0.59           |
| 19.3 | 0          | 0             | 50           | 0.298          |
| 5.1  | 0          | 0             | 100          | 0.149          |
| 1.6  | 0          | 0             | 200          | 0.074          |
|      |            |               |              |                |

#### a) Cement

Cement used in this study is Fars cement type 2, the characteristics of which are listed in Table 2.

#### Table 2

| The distribution of spec | cifications of the cement<br>Compressive str | ications of the cement<br>Compressive strength (kg/cm <sup>2</sup> ) |        |     | Initial<br>curing<br>period<br>(minute) | Specific area<br>(cm²/g) |
|--------------------------|--|--|--------|-----|---|--------------------------|
|                          | 28 days                                      | 7 days   | 3 days |     |   |                          |
| results                  | 315  | 175 10   |        | 195 | 130                                     | 2800                     |

#### b) Bentonite

Bentonite used in the manufacture of concrete is from Darin Kashan company's bentonite, the specifications of which are given in Table 3.

Table 3

The distribution of specifications of the bentonite

| characteristic | Quantity measured |
|----------------|-------------------|
| LL             | 314.5             |
| PI             | 283.3             |
| Gs             | 2.79              |
| Classification | СН                |
| Clay Fraction  | 72                |
| Silt Fraction  | 23                |
| Sand Fraction  | 1                 |
| w opt %        | 23                |
| Dry density    | 1.56              |
| SSA (m2/gr)    | 418               |
| CEC (cmol/kg)  | 68.2              |

#### c) Water

Water used in the manufacture of concrete is from drinking water of the workshop, which PH is 7.5.

## d) Mixing plan

The mixing plan and specifications of the plastic concrete of the Nargesi dam's cut-off wall are in accordance with Tables 4 and 5, which is in accordance with the wanted technical specifications of the design. The required compressive strength is considered for a 7-day age range of approximately 0.8 to 1.5 MPa and for the age of 28 days is 1.5 to 2.5 MPa and the Young's modulus for 28 days is between 200 and 400 MPa.

Table 4 The distribution of the amount of materials used to make 1 cubic meter of plastic concrete

| Consumed materials | (kg) |
|--------------------|------|
| cement             | 130  |
| bentonite          | 40   |
| water              | 382  |
| sand               | 705  |
| Pea gravel         | 520  |
| Almond gravel      | 259  |

#### Table 5

The distribution of approved mixing plan of the cut-off wall in Nargesi dam

| (Kg)Cement | (kg)Bentonite | (W/B)Water to bentonite | slump (cm) | 28 days (kg/cm <sup>2</sup> )                |                                |  |
|------------|---------------|-------------------------|------------|--|--------------------------------|--|
| weight     | weight        | proportion              |            | (kg/cm <sup>2</sup> )Compressive<br>strength | (kg/cm²) Elasticity<br>modulus |  |
| 130        | 40            | 9.55                    | 20.5       | 13.8   | 2750                           |  |

The manufacturing process of the plastic concrete in this study is as follows. The bentonite slurry was first made according to portions mentioned in the mixing scheme and turned into gelatin after 24 hours of processing. Then the other concrete-forming materials such as dry sand, gravel and cement were mixed in a betonyer for 5 minutes and then gently bentonite slurry was added. All the concrete ingredients were then mixed in the betonyer for 15 minutes. After sampling for 24 hours, the samples were kept in the mold at the laboratory temperature (20 ° C) and then the molds were opened and stored in a pond containing water. After 28 days of sampling, the samples were taken out of the pond

and the two ends of the specimens were changed to a flat surface before being put under a bentonite cracker jack in order to uniform loading by melted sulfur and then tested.

At the next step, all panels are sampled and Curinged as follows (Fig. 4).



Fig.4. Curing Concrete Samples

In Table 6, the results of pouring concrete of the cut-off wall panels of the main body of the Nargesi dam project are fully included for different ages.

| column | panel      | 11 days<br>strength | 42 days strength | 90 days strength | 11 days modulus | 42 days modulus | 90 days modulus |
|--------|------------|---------------------|------------------|------------------|-----------------|-----------------|-----------------|
|        | P1         | 14.1                | 20.5             | 26.5             | 3475            | 3711            | 4701            |
| 1      | S1<br>P2   | 14                  | 21.2             | 26.9             | 3451            | 3870            | 4735            |
| 2      | S2         | 8.1                 | 14.5             | 15.7             | 2011            | 3266            | 3810            |
| 2      | 52         | 8.4                 | 15.5             | 16.4             | 2057            | 3237            | 3923            |
| 3      | P3         | 9.2                 | 13.5             | 15.7             | 2354            | 3722            | 3925            |
| 5      | 15         | 9.1                 | 14.3             | 16.2             | 2317            | 3786            | 3978            |
| 4      | <b>S</b> 3 | 9.7                 | 13.2             | 14.2             | 2275            | 3739            | 3590            |
| +      | 35         | 9.7                 | 14.1             | 14.5             | 2259            | 3488            | 3618            |
| 5      | P4         | 13.4                | 20.4             | 21.2             | 2845            | 4242            | 4722            |
| 5      | Г4         | 13.8                | 20.3             | 21.2             | 2878            | 4217            | 4731            |
| 6      | <b>S</b> 4 | 8                   | 13.8             | 16.7             | 2178            | 3588            | 4077            |
| 0      | 54         | 8.1                 | 14.6             | 16.6             | 2190            | 3679            | 4015            |
| 7      | P5         | 13.1                | 18.4             | 23.6             | 2879            | 3510            | 4886            |
| /      | r5         | 13                  | 19.7             | 23.2             | 2894            | 3567            | 4832            |
| 8      | 8 S5       | 9.3                 | 14.6             | 18.5             | 2412            | 3011            | 4013            |
| 0      | 35         | 9.8                 | 14.8             | 18.2             | 2456            | 3072            | 3967            |
| 9      | P6         | 8.7                 | 13.9             | 16.5             | 2091            | 3319            | 4026            |
| 7      | 10         | 9.2                 | 14.2             | 16.9             | 2134            | 3368            | 4091            |
| 10     | <b>S</b> 6 | 6.6                 | 11.1             | 13.1             | 1876            | 2496            | 3385            |
| 10     | 30         | 6.5                 | 11.6             | 12.9             | 1852            | 2519            | 3353            |
| 11     | P7         | 10.5                | 19.2             | 21.5             | 2311            | 4216            | 5034            |
| 11     | Γ/         | 10.7                | 18.7             | 20.7             | 2358            | 4216            | 4976            |
| 12     | <b>S</b> 7 | 11.6                | 17.5             | 19.1             | 2445            | 3326            | 4136            |
| 12     | 57         | 11.3                | 17.2             | 19.6             | 2420            | 3300            | 4197            |
| 13     | P8         | 8.3                 | 12.6             | 15.4             | 2144            | 3160            | 3564            |
| 15     | 10         | 8.1                 | 12.9             | 14.7             | 2108            | 3177            | 3525            |
| 14     | <b>S</b> 8 | 7.6                 | 10.3             | 10.8             | 1982            | 2324            | 2546            |
| 14     | 30         | 7.1                 | 10.2             | 11.1             | 1976            | 2232            | 2553            |
| 15     | Р9         | 10.3                | 17.1             | 18.7             | 2262            | 3250            | 4004            |
| 15     | 17         | 10.3                | 16.9             | 19.2             | 2244            | 3216            | 2023            |
| 16     | <b>S</b> 9 | 11.4                | 18.6             | 20.7             | 2458            | 3590            | 3877            |
| 10     | 57         | 11.2                | 18.3             | 20.9             | 2433            | 3510            | 3991            |

Table 6 Specifications of the strength and elasticity modulus of the cut-off wall (kg/cm<sup>2</sup>)

| Table | 6 | (continued) |
|-------|---|-------------|
|       |   |             |

| column | panel       | 11 days<br>strength | 42 days strength | 90 days strength | 11 days modulus | 42 days modulus | 90 days<br>modulus |
|--------|-------------|---------------------|------------------|------------------|-----------------|-----------------|--------------------|
| 22     | <b>D</b> 10 | 6.9                 | 12.5             | 14.1             | 2108            | 3028            | 3645               |
| 33     | P18         | 7.3                 | 13.1             | 14.2             | 2145            | 3054            | 3698               |
| 24     | 610         | 13.2                | 19.7             | 24.3             | 3358            | 4296            | 5158               |
| 34     | S18         | 13.2                | 19.9             | 23.2             | 3337            | 4369            | 5053               |
| 25     | <b>D</b> 10 | 13.3                | 22.4             | 23.2             | 2755            | 4880            | 5176               |
| 35     | P19         | 13.9                | 21.9             | 23               | 2773            | 4769            | 5133               |
| 26     | 610         | 22.2                | 32.9             | 33.7             | 4247            | 6543            | 6710               |
| 36     | S19         | 22.6                | 31.8             | 33.2             | 4225            | 6385            | 6680               |
| 27     | <b>D</b> 20 | 8.2                 | 15.6             | 20.3             | 2145            | 3226            | 4002               |
| 37     | P20         | 8.1                 | 15.8             | 19.6             | 2117            | 3251            | 3975               |
| 20     | 620         | 10.4                | 18.2             | 20.7             | 2145            | 3280            | 3741               |
| 38     | S20         | 10.5                | 18.1             | 20.7             | 2133            | 3251            | 3765               |
| 20     | D21         | 5.8                 | 10.3             | 13.8             | 1157            | 2018            | 2750               |
| 39 P2  | P21         | 5.7                 | 10.4             | 13.2             | 1140            | 2037            | 2678               |
| 40 S21 | 621         | 13.1                | 18               | 19               | 2655            | 3416            | 4142               |
|        | 521         | 12.2                | 18.6             | 19.8             | 2472            | 3466            | 4168               |
|        | P22         | 5.7                 | 11               | 12.8             | 1256            | 2451            | 2715               |
| 41     | P22         | 5.8                 | 11.1             | 13               | 1289            | 2477            | 2761               |
| 42     | S22         | 7.1                 | 13.2             | 15.2             | 2547            | 3486            | 3992               |
| 42     | 522         | 7.1                 | 13.1             | 15.5             | 2553            | 3451            | 4060               |
| 42     | D22         | 8.4                 | 12.2             | 16.1             | 2320            | 2845            | 3562               |
| 43     | P23         | 8.5                 | 12               | 16               | 2351            | 2811            | 3527               |
| 4.4    | 622         | 11.2                | 18               | 22               | 2411            | 3350            | 4918               |
| 44     | S23         | 11.4                | 18.4             | 22.3             | 2487            | 3389            | 4937               |
| 45     | P24         | 6.5                 | 11.9             | 15.3             | 1622            | 2937            | 3505               |
| 45     | P24         | 6.6                 | 12.2             | 15.6             | 1688            | 2984            | 3576               |
| 46     | S24<br>S25  | 6.8                 | 11.5             | 12.6             | 2045            | 2589            | 3063               |
|        | P25         | 6.7                 | 12.2             | 12.9             | 2076            | 2655            | 3067               |
| 47     | P25         | 8.8                 | 13.7             | 16.6             | 2458            | 2864            | 3280               |
| 77     | 1 23        | 9                   | 13.6             | 16.5             | 2371            | 2851            | 3274               |
| 48     | P26         | 5.7                 | 9.7              | 11.2             | 1254            | 2176            | 2715               |

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Table 6 (continued)

| column | panel       | 11 days<br>strength | 42 days strength | 90 days strength | 11 days modulus | 42 days modulus | 90 days<br>modulus |
|--------|-------------|---------------------|------------------|------------------|-----------------|-----------------|--------------------|
| 40     | 526         | 7                   | 13.7             | 15.6             | 2122            | 3253            | 3578               |
| 49     | S26         | 7.5                 | 13.9             | 16.2             | 2160            | 3288            | 3615               |
| 50     | D27         | 7.4                 | 11.7             | 14.9             | 1506            | 2747            | 3880               |
| 50     | P27         | 7.9                 | 11.9             | 15.3             | 1547            | 2784            | 3918               |
| 51     | 807         | 6.9                 | 11.4             | 15.3             | 1541            | 2840            | 3910               |
| 51     | S27         | 6.8                 | 11.5             | 15.6             | 1522            | 2879            | 3945               |
| 50     | <b>D</b> 20 | 7                   | 12.4             | 14.1             | 1864            | 2654            | 3980               |
| 52     | P28         | 7                   | 12.3             | 14.2             | 1850            | 2689            | 3994               |
| 52     | 630         | 7.3                 | 12.6             | 15.6             | 1864            | 2959            | 4145               |
| 53     | S28         | 7.3                 | 12.8             | 15.5             | 1877            | 2981            | 4110               |
| 54     | 620         | 10.8                | 17.4             | 22.1             | 2881            | 3285            | 3904               |
| 54     | S29         | 10.6                | 16.8             | 22.5             | 2842            | 3144            | 4000               |
| 55     | P30         | 7.1                 | 11.2             | 15.1             | 2091            | 2784            | 3605               |
| 55     | P30         | 7.2                 | 11.7             | 15.2             | 2104            | 2800            | 3634               |
| 56     | <b>S</b> 30 | 7.9                 | 13.4             | 14.1             | 1981            | 3149            | 3223               |
| 50     | 350         | 7.8                 | 13.3             | 14               | 1972            | 3014            | 3212               |
| 57     | P31         | 6.1                 | 11.8             | 14.7             | 2118            | 2626            | 4053               |
| 57     | P31         | 6                   | 11.6             | 14.6             | 2147            | 2587            | 4018               |
| 58     | <b>S</b> 31 | 15.2                | 29.8             | 34.9             | 3284            | 5449            | 5910               |
| 50     | 351         | 15.5                | 29.6             | 35.5             | 3301            | 5486            | 5848               |
| 50     | D22         | 8.1                 | 11.9             | 16.1             | 2054            | 2771            | 3604               |
| 59     | P32         | 8.3                 | 11.9             | 15.9             | 2076            | 2759            | 3533               |
| 60     | P33         | 9.6                 | 20.6             | 23.4             | 2570            | 4221            | 4533               |
| 00     | r 55        | 9.5                 | 21.3             | 23               | 2550            | 4365            | 4517               |
| 61     | <b>S</b> 33 | 6.7                 | 12.8             | 13.2             | 1927            | 3003            | 3408               |
| 01     | 355         | 6.8                 | 12.9             | 13.6             | 1905            | 3010            | 3424               |
| 62     | P34         | 7                   | 12.4             | 18.3             | 1978            | 2987            | 3688               |
| 02     | r 34        | 6.9                 | 12.7             | 18               | 1924            | 3069            | 3645               |
| 63     | <b>S</b> 34 | 4.6                 | 8.5              | 9.5              | 1124            | 2579            | 3026               |
| 03     | 334         | 4.7                 | 8.3              | 9.6              | 1109            | 2410            | 3040               |
| 64     | P35<br>S35  | 8.4                 | 13.5             | 18.6             | 2291            | 3047            | 4009               |
|        | P36         | 8.3                 | 13.4             | 18.4             | 2285            | 3015            | 3947               |

| Table 6 | (continued) |
|---------|-------------|
|---------|-------------|

| column     | panel        | 11 days<br>strength | 42 days strength | 90 days strength | 11 days modulus | 42 days<br>modulus | 90 days modulus |
|------------|--------------|---------------------|------------------|------------------|-----------------|--------------------|-----------------|
| (5         | 626          | 7.9                 | 12.7             | 13.7             | 2178            | 3354               | 4157            |
| 65         | <b>S</b> 36  | 8                   | 12.5             | 14               | 2201            | 3316               | 4165            |
| 66         | P37          | 6.7                 | 13.8             | 15.6             | 1794            | 3315               | 3641            |
| 66         | P37          | 6.7                 | 14.1             | 15.9             | 1758            | 3420               | 3687            |
| (7         | 627          | 6.7                 | 10               | 12.9             | 1830            | 2415               | 3248            |
| 67         | S37          | 6.9                 | 10.6             | 13               | 1843            | 2466               | 3265            |
| 60         | <b>D2</b> 0  | 9                   | 14.9             | 17.4             | 2410            | 3324               | 3824            |
| 68         | P38          | 8.9                 | 14.9             | 17.5             | 2378            | 3309               | 2851            |
| <i>c</i> 0 | 620          | 7                   | 12.1             | 12.8             | 1985            | 2924               | 3296            |
| 69         | S38          | 7                   | 12.5             | 13.3             | 1921            | 3084               | 3484            |
| =0         |              | 6.8                 | 14.2             | 16.7             | 2201            | 3488               | 4650            |
| 70         | P39          | 6.9                 | 14               | 16.8             | 2232            | 3540               | 4691            |
|            |              | 6.7                 | 11.6             | 15.9             | 2410            | 2740               | 3845            |
| 71         | I \$39       | 6.8                 | 11.8             | 16.2             | 2317            | 2755               | 3885            |
| = 0        | 72 P40       | 9.2                 | 15.9             | 22.1             | 2321            | 3131               | 3857            |
| 12         |              | 9.1                 | 16.3             | 21.9             | 2329            | 3254               | 3836            |
| =0         | <b>6</b> 4 6 | 5.2                 | 9.3              | 11.8             | 1250            | 2684               | 3335            |
| 73         | S40          | 5.2                 | 9.4              | 11.7             | 1135            | 2624               | 3324            |
|            |              | 12.25               | 19.3             | 22.68            | 2380            | 4319               | 4684            |
| 74         | P41          | 12.18               | 18.62            | 23.22            | 2344            | 4335               | 4771            |
|            |              | 9.3                 | 15.7             | 17.2             | 2743            | 3314               | 3678            |
| 75         | S41          | 9.1                 | 15.9             | 17               | 2712            | 3361               | 3645            |
|            |              | 6.6                 | 12.2             | 14.2             | 2205            | 2916               | 3352            |
| 76         | P42          | 6.6                 | 12.3             | 14.7             | 2187            | 2934               | 3378            |
|            |              | 7                   | 13.9             | 14.9             | 1710            | 3256               | 4018            |
| 77         | S42          | 6.9                 | 13.7             | 15.1             | 1689            | 3231               | 4054            |
|            |              | 8.7                 | 14.9             | 19.6             | 2236            | 3878               | 4467            |
| 78         | P43          | 8.5                 | 14.8             | 19.5             | 2219            | 3889               | 4418            |
|            |              | 5.7                 | 10.4             | 12.4             | 1327            | 2350               | 2811            |
| 79         | S43          | 5.7                 | 10.5             | 12.7             | 1318            | 2389               | 2839            |
|            |              | 10.4                | 14.4             | 17.8             | 2615            | 3807               | 4101            |
| 80         | P44          | 10.5                | 14.3             | 18.1             | 2628            | 3756               | 4123            |

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Table 6 (continued)

| column | panel       | 11 days<br>strength | 42 days strength | 90 days strength | 11 days modulus | 42 days<br>modulus | 90 days modulus |      |
|--------|-------------|---------------------|------------------|------------------|-----------------|--------------------|-----------------|------|
| 81     | S44         | 8                   | 12               | 13.8             | 2011            | 2619               | 2841            |      |
| 01     | 544         | 7.9                 | 12.3             | 14.2             | 2008            | 2634               | 2875            |      |
| 82     | P45         | 9.8                 | 17               | 20.9             | 2866            | 3769               | 5279            |      |
| 02     | F4J         | 9.4                 | 17.2             | 21.5             | 2789            | 3775               | 5344            |      |
| 83     | S45         | 6.2                 | 10.8             | 11.8             | 1675            | 2413               | 3047            |      |
| 65     | 345         | 6.3                 | 10.9             | 11.7             | 1689            | 2459               | 3015            |      |
| 84     | P46         | 7.1                 | 12.9             | 14.5             | 1775            | 3159               | 3335            |      |
| 64     | P40         | 7                   | 13               | 14.6             | 1738            | 3184               | 3361            |      |
| 85     | S16         | 7.2                 | 11.9             | 15.4             | 1728            | 2819               | 3476            |      |
| 63     | S46         | 7.3                 | 12               | 15               | 1804            | 2841               | 3418            |      |
| 86     | P47         | 5.4                 | 10.7             | 12.7             | 1587            | 2336               | 3135            |      |
| 80     | P47         | 5.3                 | 10.9             | 12.9             | 1501            | 2345               | 3163            |      |
| 87     | 647         | 6.5                 | 10.7             | 13.8             | 1744            | 3210               | 3684            |      |
| 87     | S47         | 6.4                 | 10.9             | 13.6             | 1775            | 3277               | 3621            |      |
| 00     | P48         | 6.6                 | 12               | 16.1             | 2257            | 2680               | 3498            |      |
| 88     |             | 00 F40              | 5.8              | 11.9             | 16.1            | 2116               | 2627            | 3487 |
| 20     | 89 S48      | C 649               | 9.6              | 14               | 17.1            | 2927               | 3528            | 4125 |
| 89     |             | 9.9                 | 13.9             | 17.2             | 2956            | 3504               | 4134            |      |
| 90     | <b>D</b> 40 | 3.9                 | 9.4              | 10.8             | 1413            | 2889               | 3219            |      |
| 90     | P49         | 4.9                 | 10.3             | 10.9             | 1660            | 3056               | 3231            |      |
| 01     | 640         | 10.9                | 14.5             | 17               | 2237            | 3153               | 3561            |      |
| 91     | S49         | 10.8                | 15.2             | 17.1             | 2185            | 3264               | 3597            |      |
| 02     | D50         | 17.2                | 30.1             | 37.8             | 3574            | 5144               | 5758            |      |
| 92     | P50         | 17.2                | 31               | 38.5             | 3551            | 5207               | 5992            |      |
| 02     | 850         | 9.6                 | 18.3             | 18.6             | 2213            | 3325               | 3490            |      |
| 93     | S50         | 9.4                 | 18.4             | 19.1             | 2181            | 3357               | 3520            |      |
| 04     | DC 1        | 7.4                 | 12.8             | 14.5             | 2082            | 2724               | 3214            |      |
| 94     | P51         | 7.2                 | 12.8             | 14.5             | 2043            | 2739               | 3198            |      |
| 05     | 071         | 8.5                 | 12.4             | 14.1             | 2096            | 2915               | 3273            |      |
| 95     | S51         | 8.6                 | 12.7             | 14               | 2113            | 2942               | 3163            |      |
| 0.4    | D72         | 5.4                 | 9.5              | 11.1             | 1884            | 2331               | 2569            |      |
| 96     | P52         | 5.2                 | 9.8              | 11               | 1827            | 2367               | 2535            |      |

Table 6 (continued)

| column | panel | 11 days strength | 42 days strength | 90 days strength | 11 days<br>modulus | 42 days<br>modulus | 90 days<br>modulus |
|--------|-------|------------------|------------------|------------------|--------------------|--------------------|--------------------|
| 97     | 852   | 7.1              | 14.7             | 15.8             | 1985               | 3453               | 3554               |
|        |       | 6.9              | 15               | 16.3             | 1927               | 3485               | 3669               |
| 98     | P53   | 19               | 32.5             | 50.2             | 3498               | 5749               | 6325               |
|        |       | 18               | 33.3             | 50.3             | 3385               | 5801               | 6385               |
| 99     | \$53  | 5.7              | 11.4             | 11.7             | 1829               | 2929               | 2981               |
|        |       | 5.6              | 11.5             | 11.8             | 1810               | 2934               | 3004               |
| 100    | P54   | 9.1              | 17.8             | 18.3             | 2181               | 3442               | 3650               |
|        |       | 9                | 17.7             | 18.7             | 2064               | 3413               | 3698               |
| 101    | S54   | 14.1             | 22.4             | 24.9             | 3209               | 4861               | 5017               |
|        |       | 13.4             | 22.3             | 25.1             | 3188               | 4863               | 5043               |
| 102    | P55   | 11.9             | 19.6             | 21.7             | 2760               | 3884               | 4446               |
|        |       | 11.6             | 19.7             | 21.5             | 2717               | 3985               | 4438               |
| 103    | S55   | 16.3             | 27.1             | 38               | 3220               | 5210               | 5941               |
|        |       | 16.6             | 26.4             | 37.1             | 3301               | 5180               | 5774               |
| 104    | P56   | 10.2             | 15.9             | 18.8             | 2155               | 3196               | 3649               |
|        |       | 9.7              | 15.7             | 18.9             | 2099               | 3120               | 3688               |
| 105    | S56   | 12               | 19.5             | 23.9             | 2675               | 3807               | 4207               |
|        |       | 11.8             | 19.6             | 24.3             | 2641               | 3795               | 4212               |
| 106    | P57   | 7.4              | 15.3             | 18.6             | 2138               | 3391               | 3789               |
|        |       | 7.2              | 14.9             | 17.9             | 2098               | 3310               | 3704               |
| 107    | S57   | 14.7             | 23.1             | 24.6             | 3528               | 4108               | 4510               |
|        |       | 14.9             | 22.5             | 24.8             | 3567               | 4179               | 4535               |
| 108    | P58   | 8.3              | 15.3             | 15.7             | 2171               | 3420               | 3619               |
|        |       | 8.1              | 15.2             | 16.3             | 2157               | 3392               | 3811               |

## 2.Objectives of the Results' Evaluation

The purpose of the results evaluation is to analyze the results of plastic concrete statistically at this stage, and find relationships that can be very important. One of the important properties of plastic concrete is a significant increase in strength and elastic modulus over time. This important issue is a) **Average** 

The simplest method of statistical analysis to examine the result of generating a product, which is created from the production of identical components, is to use the average result of products. In the method of constructing the cut-off wall, which often ignored by designers. For the importance of this topic and finding highly effective relationships with regard to the strength and elastic modulus of plastic concrete, a statistical analysis on the results of experiments was carried out on the plastic concrete cut-off wall of Nargesi dam.

consists of joining the panels, the result of the strength average and elastic modulus provides the appropriate basic information of the cut-off wall's behavior (numbers 11.42 and 90 are concrete ages).

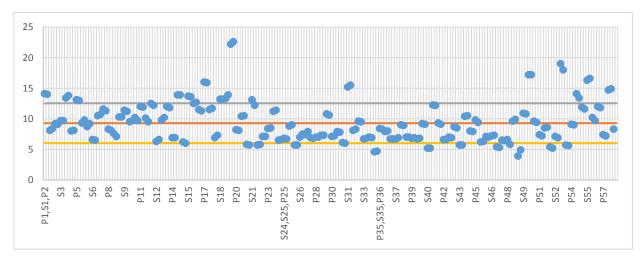
$$\bar{\sigma}_{11} = 9.296 \frac{kg}{cm^2} \qquad \overline{E}_{11} = 2283.685 \frac{kg}{cm^2} \\ \bar{\sigma}_{42} = 15.51 \frac{kg}{cm^2} \qquad \overline{E}_{42} = 3381.718 \frac{kg}{cm^2} \\ \bar{\sigma}_{90} = 18.217 \frac{kg}{cm^2} \qquad \overline{E}_{90} = 3926.157 \frac{kg}{cm^2} \\ \overline{E}_{90} = 3926.157 \frac{kg}{cm^2} \\ \bar{\sigma}_{90} = 18.217 \frac{kg}{cm^2} \qquad \overline{E}_{90} = 3926.157 \frac{kg}{cm^2} \\ \bar{\sigma}_{90} = 18.217 \frac{kg}{cm^2} \qquad \overline{E}_{90} = 3926.157 \frac{kg}{cm^2} \\ \bar{\sigma}_{90} = 18.217 \frac{$$

Since the type of cement of the type 2 cement was used in the construction of the cut-off wall's plastic concrete in Nargesi dam, the 42-day results are equivalent to the 28-day results of concrete with type 1 cement. Therefore, according to the average results of 42 days, its compliance with the instruction of the concrete construction design as well as the provisions of publication 13 (filler materials for cut-

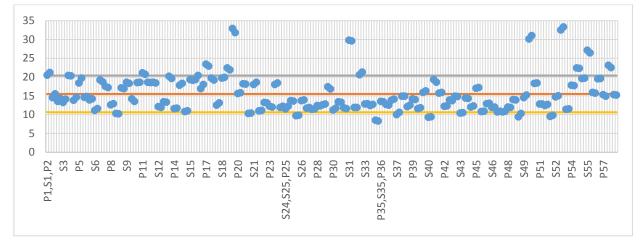
## **b)Standard deviation**

Since the algebraic aggregation of the data in the mean method causes the uncertainty of the distance between the results and the average or production standard, in other words, the negative and positive distance between the results and mean may go to zero, but each of them alone is unacceptable, therefore, the standard deviation method is used to evaluate the results. The calculations in this method off walls construction in accordance with B51 Bulletin of the ICOLD letter) based on a 28-day compressive strength of plastic concrete is equal to15 kg / cm2 (1.5 MPa) and an elastic modulus is equal to 4 to 5 times of the average modulus of the drilling site (Approximately 4000 kg / cm 2 in this project) confirms the proper achievement of the average result based on the criterions of the plan.

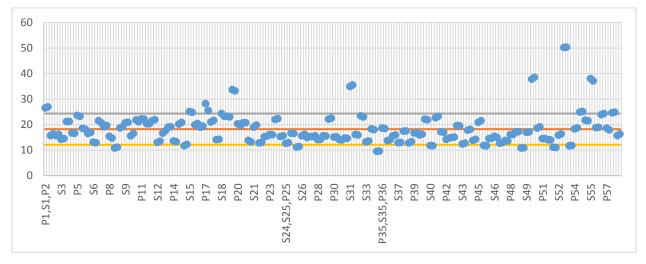
are based on the square cloth of the difference between each result and the mean, and it defines the error value in the results. In the tables below, the standard deviation, mean and the distribution of results based on the lifetime of the plastic concrete are shown for compressive strength and elasticity modulus.



(a) Compressive strength of 11-day age

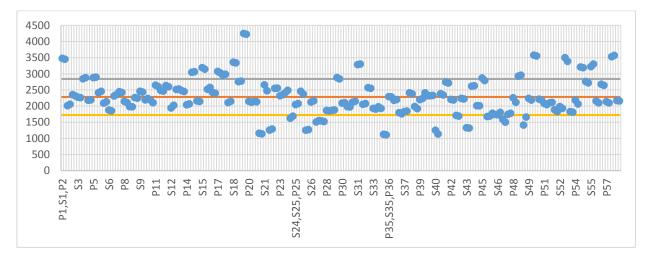


(b) Compressive strength of 42-day age

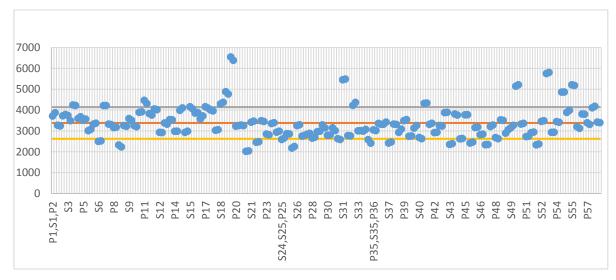


(c) Compressive strength of 90-day age

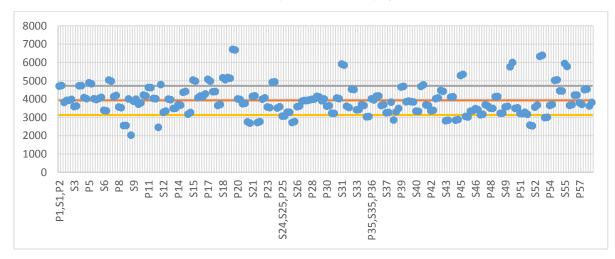
Fig.5. Compressive strength in different ages



(a) Elasticity modulus of 11-day age



(b) Elasticity modulus of 42-day age



(c) Elasticity modulus of 90-day age

Fig. 6. Elasticity modulus in different ages

If we show the standard deviation with the letter e, we will have:

$$e\sigma_{11} = \pm 3.21 \frac{kg}{cm^2} \qquad eE_{11} = \pm 558.751 \frac{kg}{cm^2} \\ e\sigma_{42} = \pm 4.81 \frac{kg}{cm^2} \qquad eE_{42} = \pm 758.772 \frac{kg}{cm^2} \\ e\sigma_{90} = \pm 6.11 \frac{kg}{cm^2} \qquad eE_{90} = \pm 795.47 \frac{kg}{cm^2} \\ eF_{90} = \pm 700 \frac{kg}{cm^2} \\ eF$$

According to the above diagrams, more than 90% of the results are within the standard deviation range.

## b) Regression Line

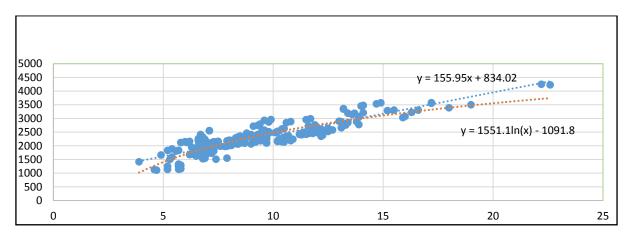
In statistical models, regression analysis is a statistical process for estimating relationships between variables. This method involves many techniques for modeling and analyzing specific and unique variables when focusing on relationships between dependent variable and one or more independent variables. Regression analysis specifically helps to understand how the value of the dependent variable varies by changing each of the independent variables and by the constancy of other independent variables.

The most common use of regression analysis is the conditional and mathematical expectation's estimation of the dependent variable of independent determinant variables, which is equivalent to the mean value of the dependent variable when the independent variables are constant. Its least use is the focus on percentile or spatial parameters of the conditional distribution of the dependent variable from a given independent variable. In all cases, the goal is to estimate a function of independent variables that is called regression function. In regression analysis, determining the dispersion of the dependent variable around the regression function is considered, which can be explained by a probability distribution.

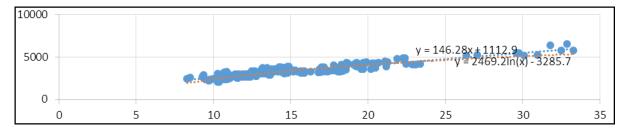
Regression analysis has been widely used for prediction. Regression analysis is also used to understand the relationship between independent and dependent variables and the form of these relationships. Under certain conditions, this analysis can be used to infer excellent relationships between independent and dependent variables.

Many techniques for regression analysis have been developed. Familiar methods such as linear regression and least squares, which are parametric, are actually estimated in this regression function under a limited number of unknown parameters of the data.

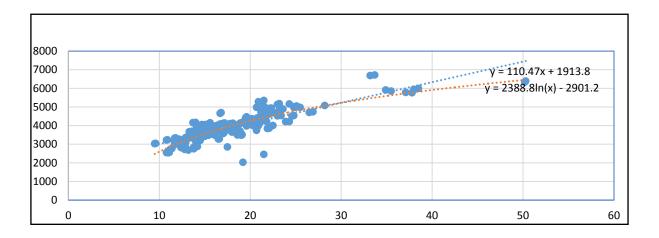
Analysis of the elasticity modulus function relative to the compressive strength based on the lifetime of the concrete is provided on the basis of the method of drawing and calculation of the regression line and the exponential enveloping curve for the results as follows:



(a) The regression line and the strength- elasticity modulus envelope curve of the 11-day age



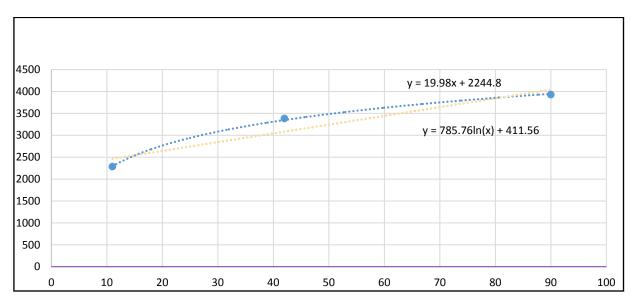
(b) The regression line and the strength- elasticity modulus envelope curve of the 42-day age



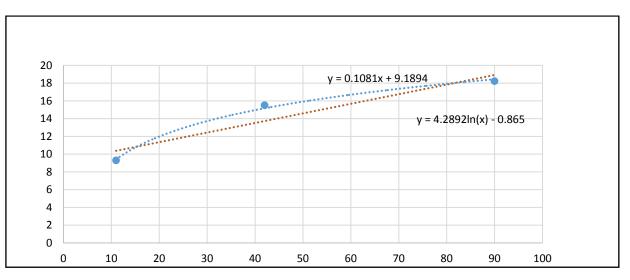
(c) The regression line and the strength- elasticity modulus envelope curve of the 90-day age elastic

Fig. 7. The regression lines and the compressive strength- elasticity modulus envelope curves

Analysis of the elasticity modulus function in relation to time, as well as compressive strength function in relation to time, is presented by drawing and calculating the regression line and the exponential enveloping curve for the results as follows:



(a) The regression line and the time- elasticity modulus envelope curve



(b) The regression line and the time- compressive strength envelope curve

Fig. 8. The regression lines and the time-compressive strength and time-elasticity modulus envelope curves

#### **6.Discussion**

There is usually a great deal between the time of construction of the wall of the clay and the time of the operation of the dam, and the determination of the behavioral parameters of the plastic concrete is very important in the operation.

In line with most works, (e. g., ICOLD [4]) figure 18, it has been revealed that strength of plastic concrete increases linearly over time, and even after 1000 days, its strength is increasing linearly. And also similarly in a research (Abbaslou et al. [2]), the below results are presented.

Between compressive strength of 7 days and compressive strength of 28 and 90 days, according to the regression coefficient, more than 0.95 linear relations dominate. The results show a linear relationship between the 28-day tensile strength and the 90-day tensile strength, with regression coefficients greater than 0.98. Using exponential functions, one can find a relation with the values of the regression coefficient greater than 0.98 for converting the compressive strength of 28 days and 90 days to their equivalent tensile strengths. It is clear from the above results that considering such a characteristic of plastic concrete, it can be very important to estimate the strength of the concrete over time.

In contrast to other works (e. g., Abbaslou, et al. [1]; Abbaslou, et al. [2]; Aman, et al. [3]; Falaki [17]; Gholipour [15]; ICOLD [4]; Kazemian, et al [14];

#### 7. Conclusions

The following results can be deduced from the above diagrams:

Increase in the strength and elasticity modulus of the plastic concrete after the 90-day life of the concrete has continued significantly (more than 2 times) in accordance with the abacus (Fig-18) presented in the B51 Bulletin of ICOLD letter.

The elastic modulus of growth rate due to the increase in the time duration is lower than the growth of the compressive strength, and, in other  $\sigma = 4.289 \ln(2000)$ -0865

$$\sigma = 31.73 \, {^{kg}/_{cm^2}}$$

Pashazadeh [5]) the present paper revealed relationships for strength and modulus of elasticity in older ages. In this research, it was tried to provide empirical relations based on what happened at the implementation stage, so that it can be used in a practical work.

words, the plasticity of the concrete is less changed over time.

Considering that nowadays due to various reasons such as on timely support financing of projects and the time consumption of the project's embankment operations, this project is about 5 years after the construction of the cut-off wall (about 2000 days later than the average run time of the cut-off wall) according to the exponential curve of the strengthtime chart, the prediction value is as follows:

According to the elastic modulus-strength enveloping curve of 90 days, the modulus prediction value for 31.73 kg

strength can be calculated as follows:

$$E = 2388.8 \ln(31.73) - 2901.2^{kg} / cm^{2}$$
$$E = 5357.5^{kg} / cm^{2}$$

On the other hand, the value of the elastic modulus can be calculated according to the module-time enveloping

curve formula for 2000 days as follows:

$$E = \frac{785}{86 \ln(2000)} + 411.56^{kg} / cm^{2}$$
$$E = 6384.04^{kg} / cm^{2}$$

According to the descriptions at the beginning of the discussion, the regression line based on the effect of independent and dependent variables on predicting the value of the function and the probability distribution with two different methods, the results of calculating the elastic modulus are predictable for 2000 days with a minimum of 5,357 and a maximum of 6,384 kg / m 2.Due to the fact that in analyzes

designers usually treated plastic concrete according to conventional concrete, and also with regard to the matters mentioned in the previous paragraphs, in the conclusion plastic concrete behavior is completely different from conventional concrete and the relations mentioned in the above paragraph can be very important and used in analyzes for the correct behavior of plastic concrete.

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